

Case Studies in Window Condensation

BCBEC Seminar – November 12, 2015

Alex McGowan, P.Eng., Levelton Consultants Ltd.

Outline of Presentation

- Introduction – Theory and Tools
- Case Study 1 – Designing the Problem in
- Case Study 2 – Designing the Problem out
- Case Study 3 – Building the Problem in
- Case Study 4 – Solving the Problem via litigation

Condensation on Windows



Case Studies in Window Condensation

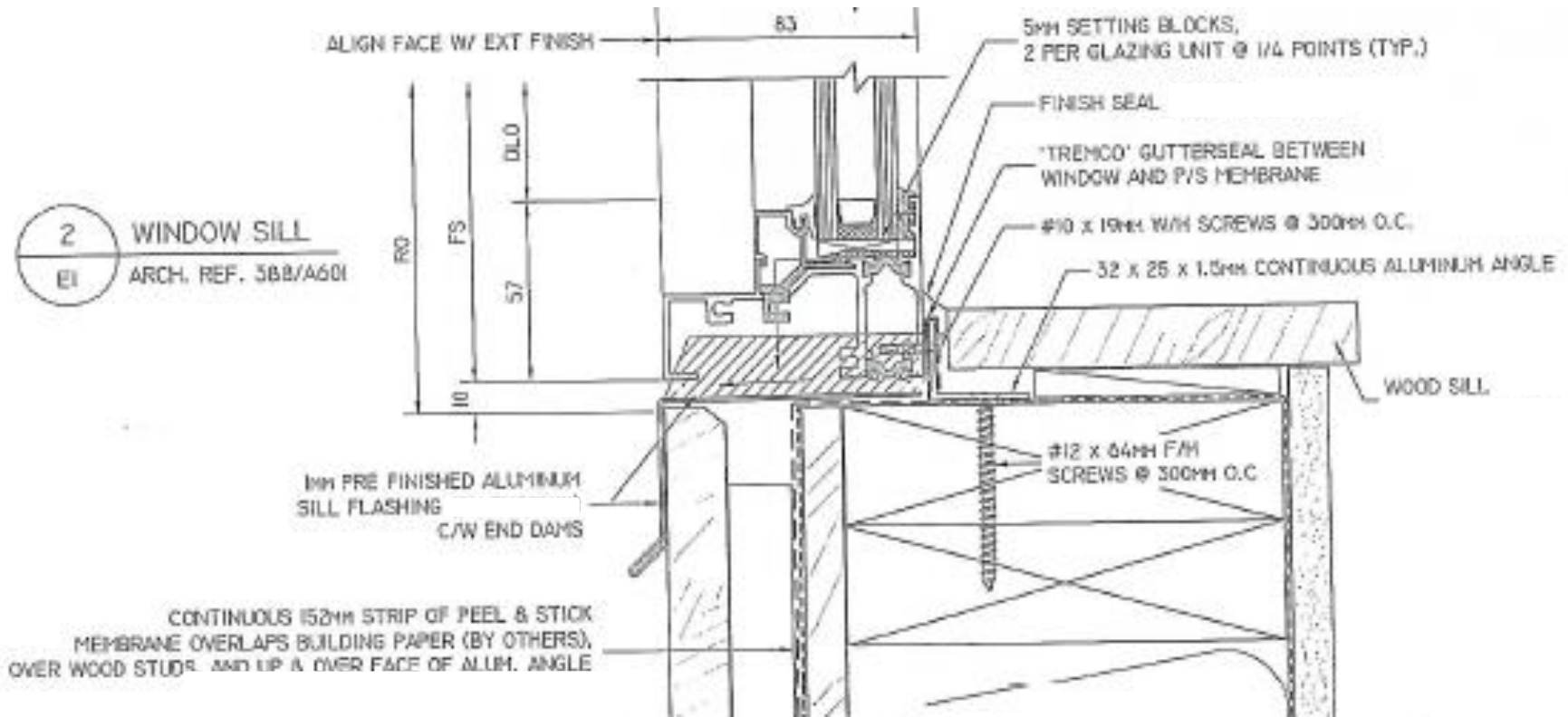
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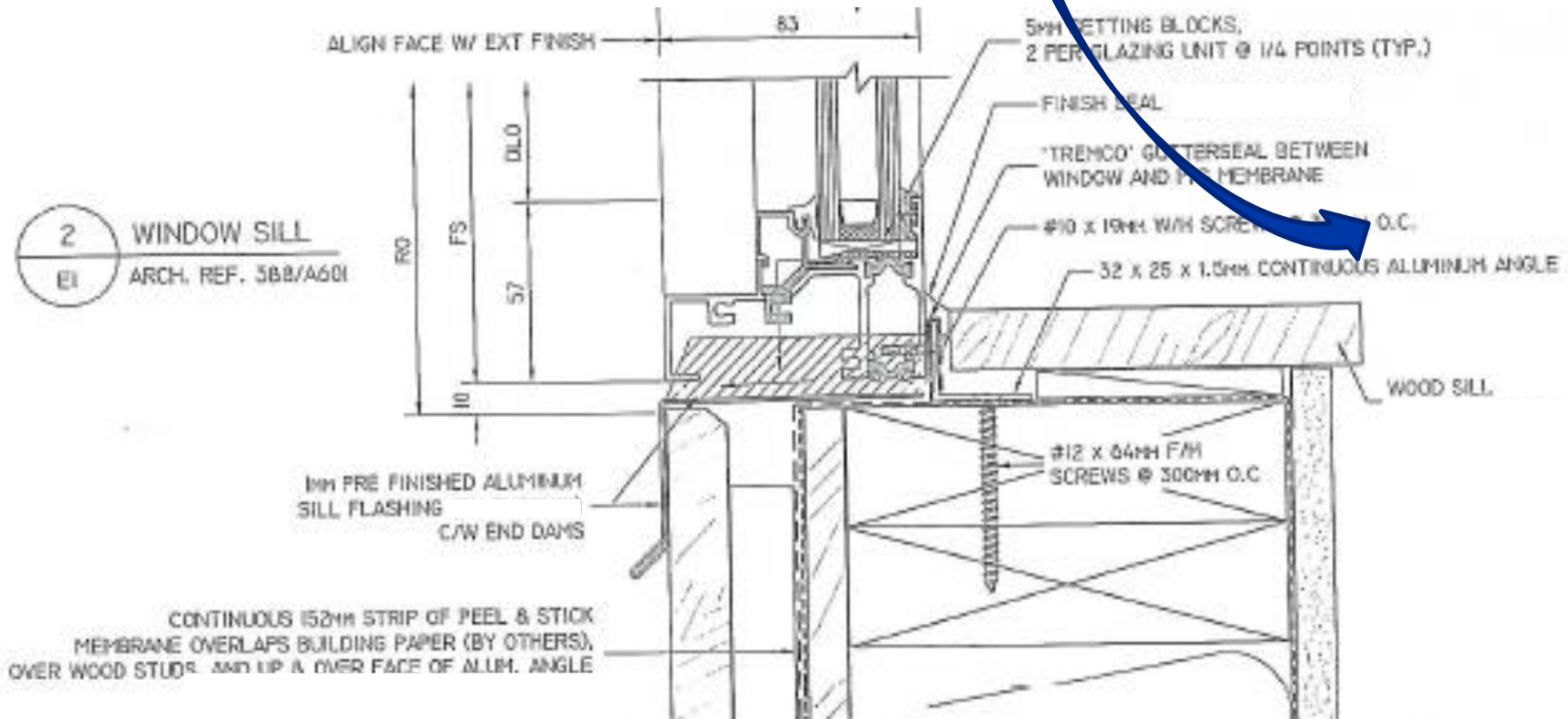
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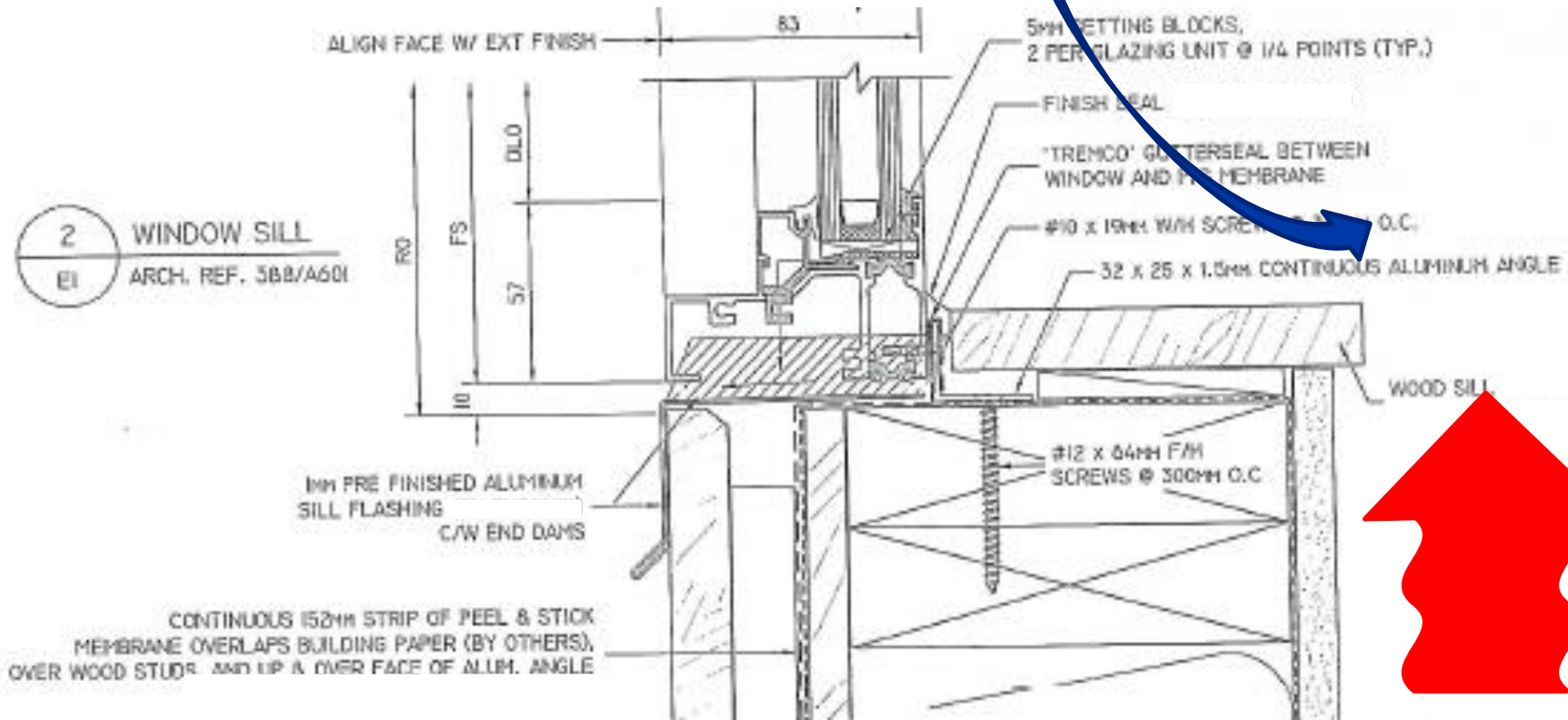
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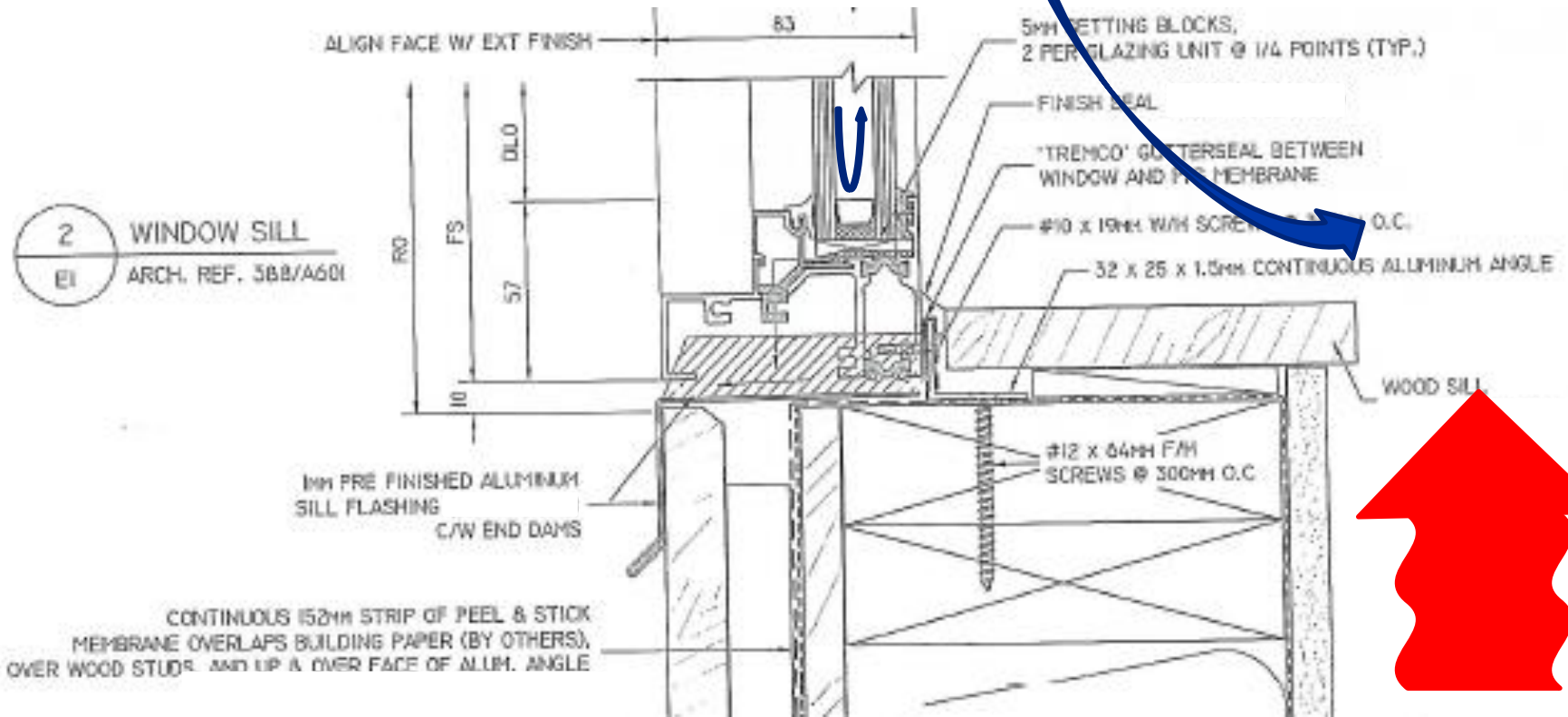
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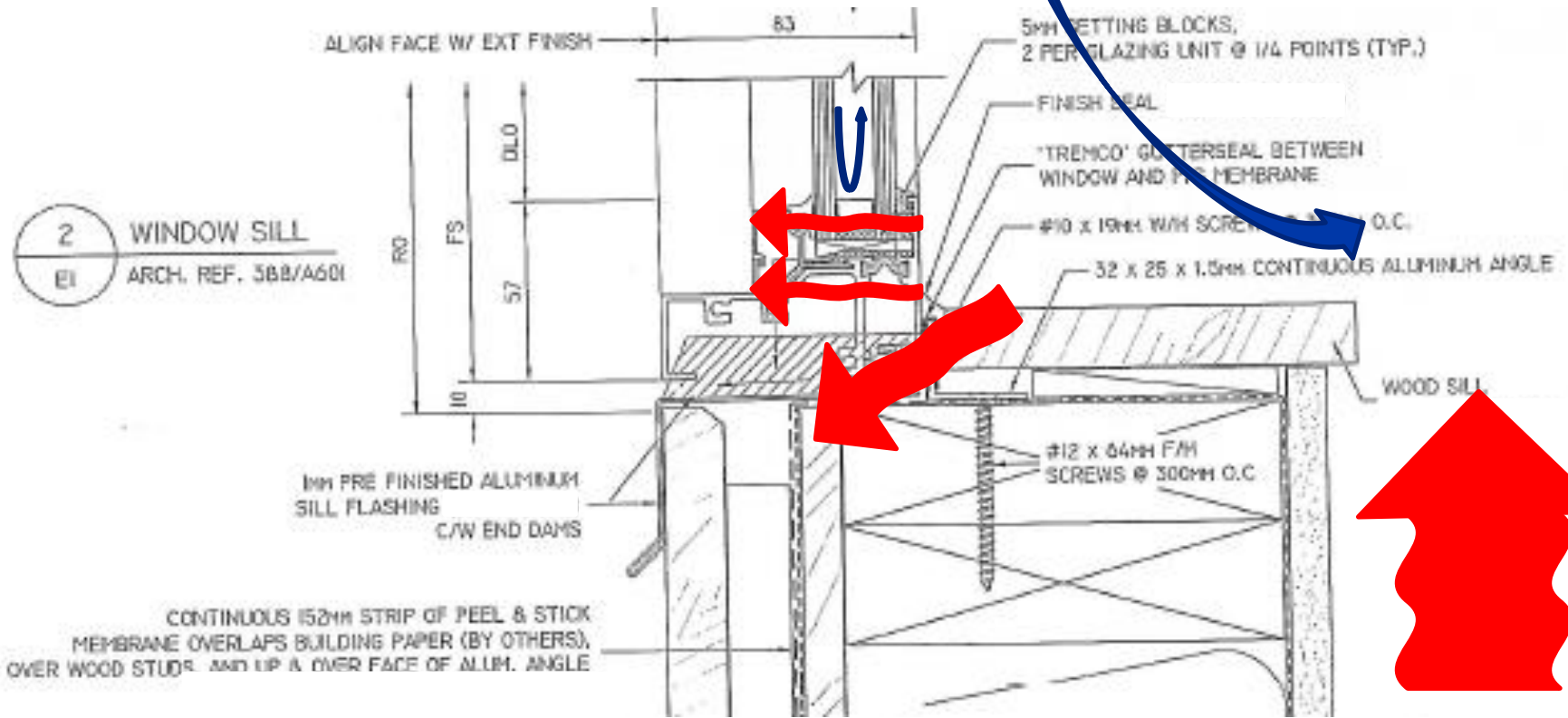
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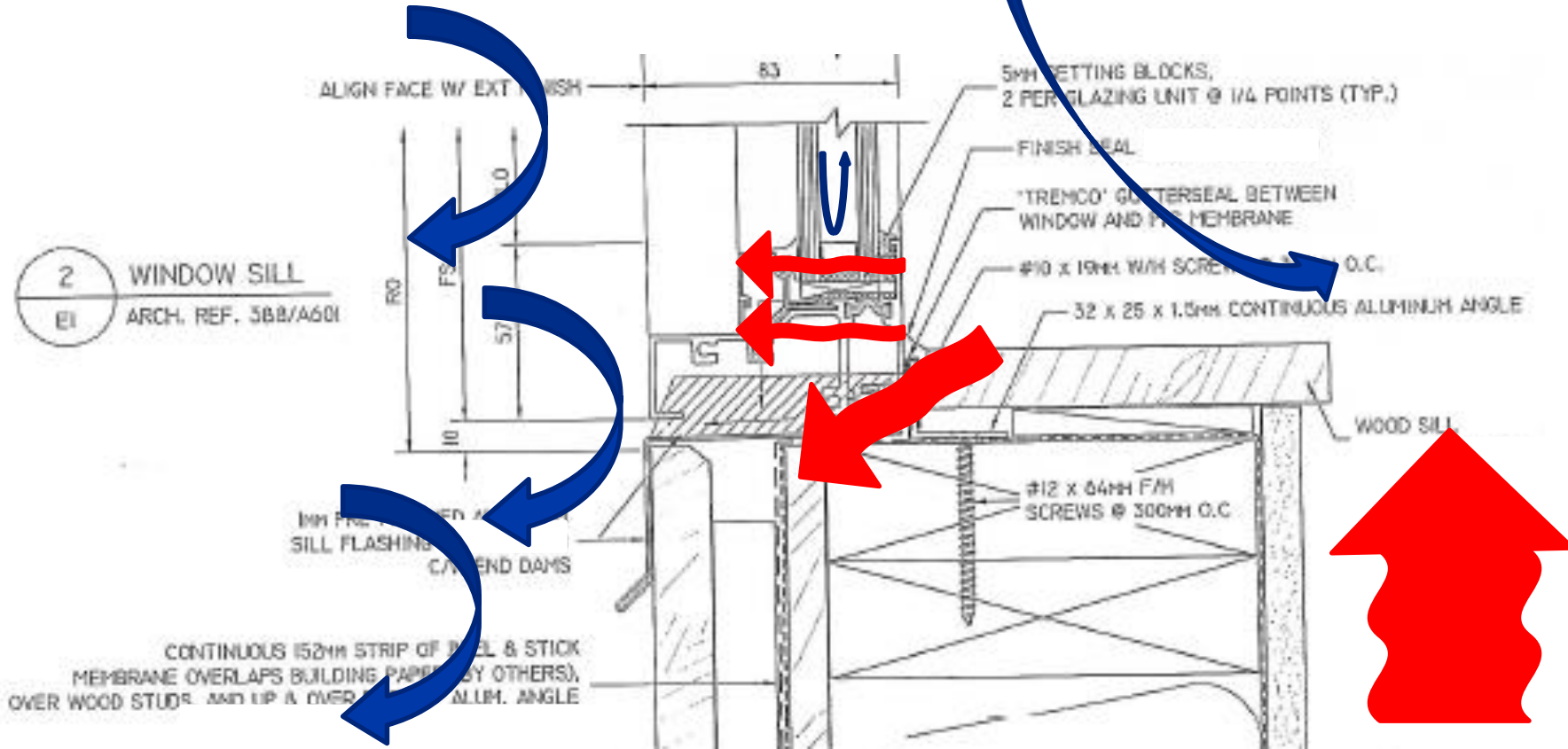
Condensation on Windows



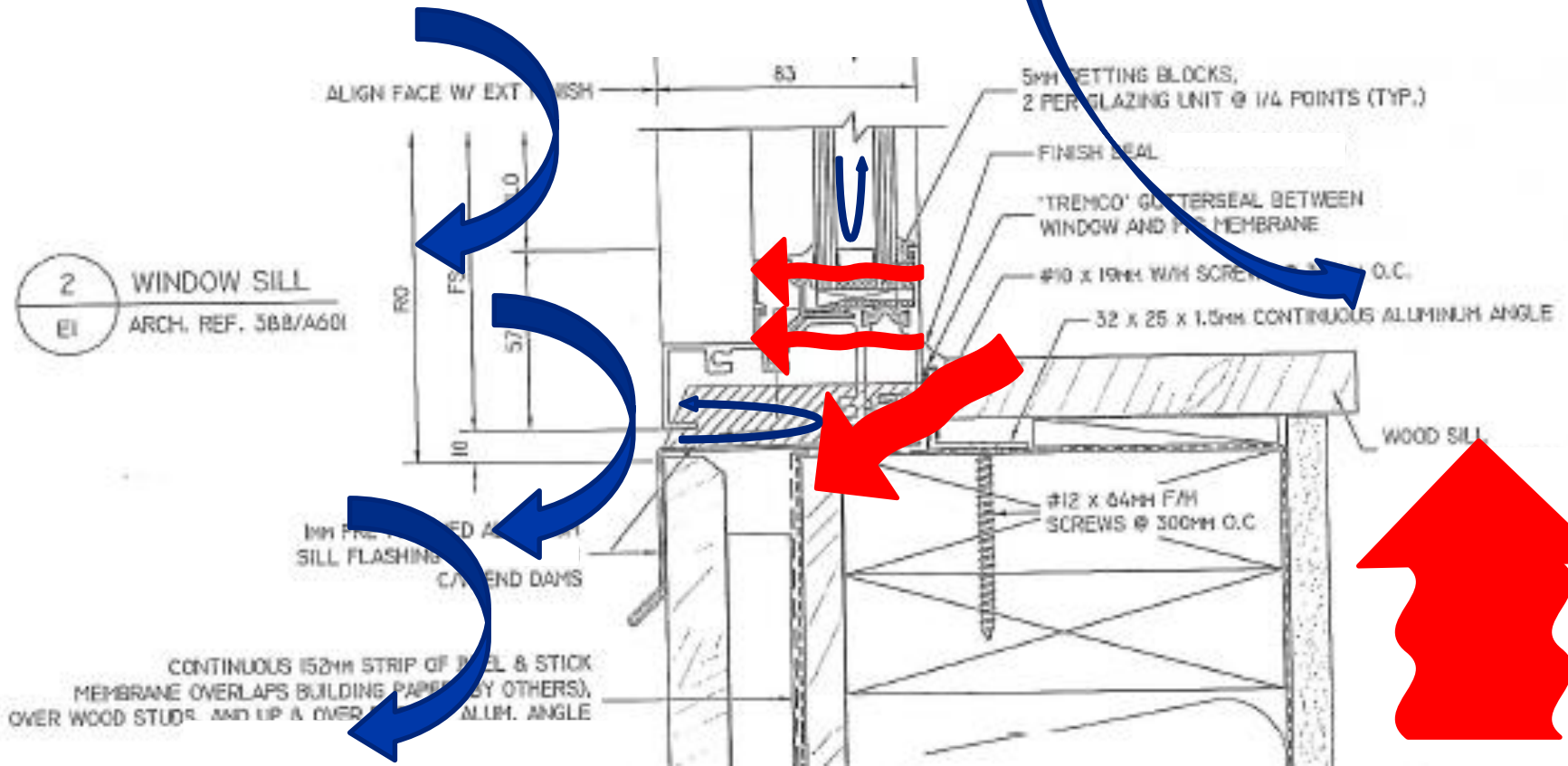
Condensation on Windows



Condensation on Windows



Condensation on Windows

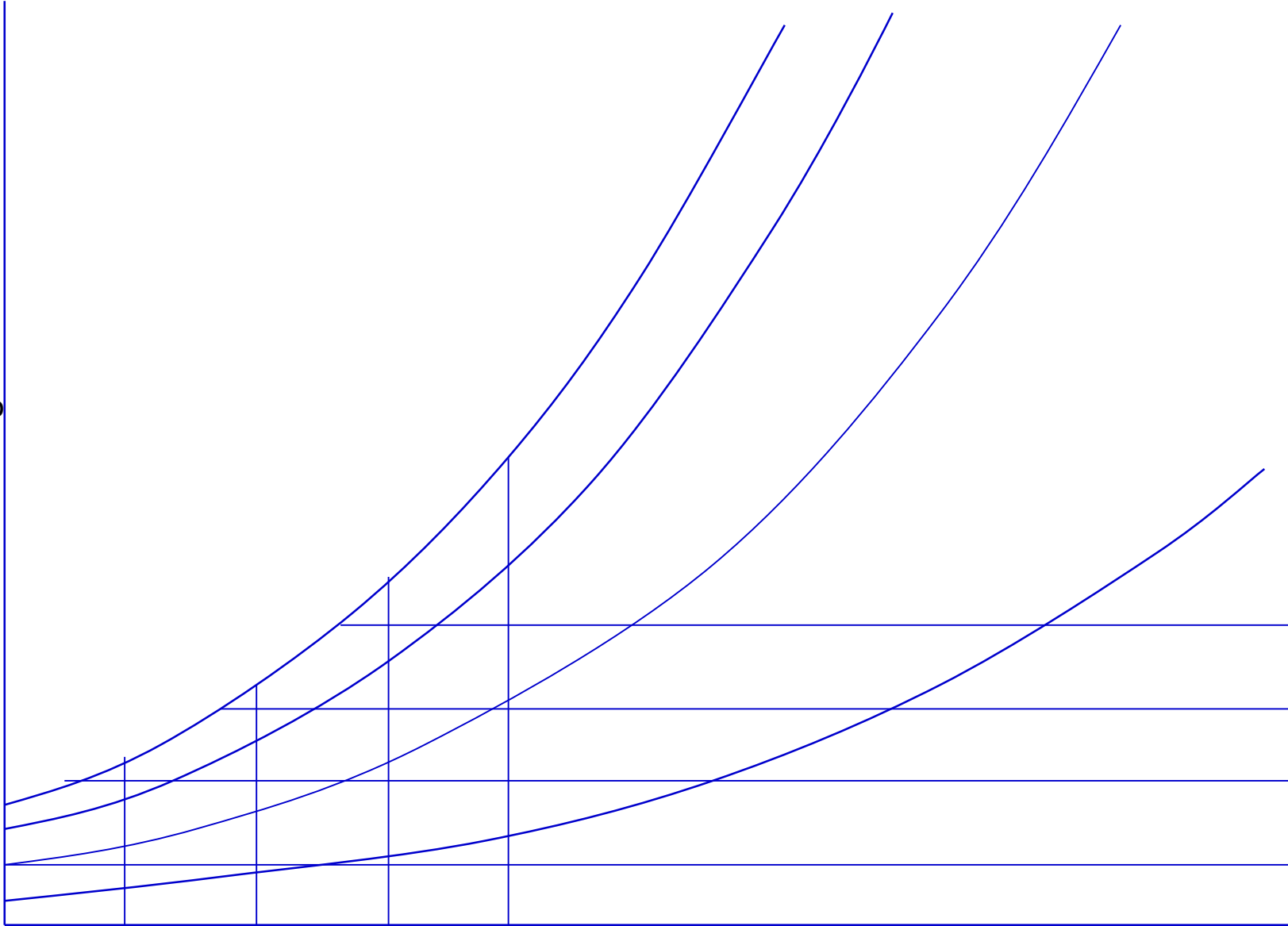


Moisture level in air increasing →

Air temperature increasing →

Moisture level in air increasing →

Air temperature increasing →





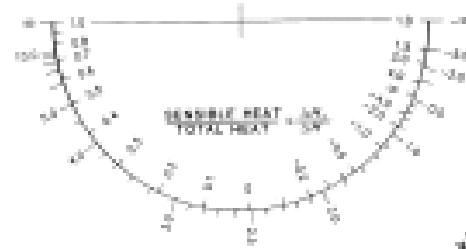
ASHRAE PSYCHROMETRIC CHART NO. 1

NORMAL TEMPERATURE SEA LEVEL

BAROMETRIC PRESSURE: 101.325 kPa

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EXAMPLES:
SENSIBLE HEAT: 100
TOTAL HEAT: 100

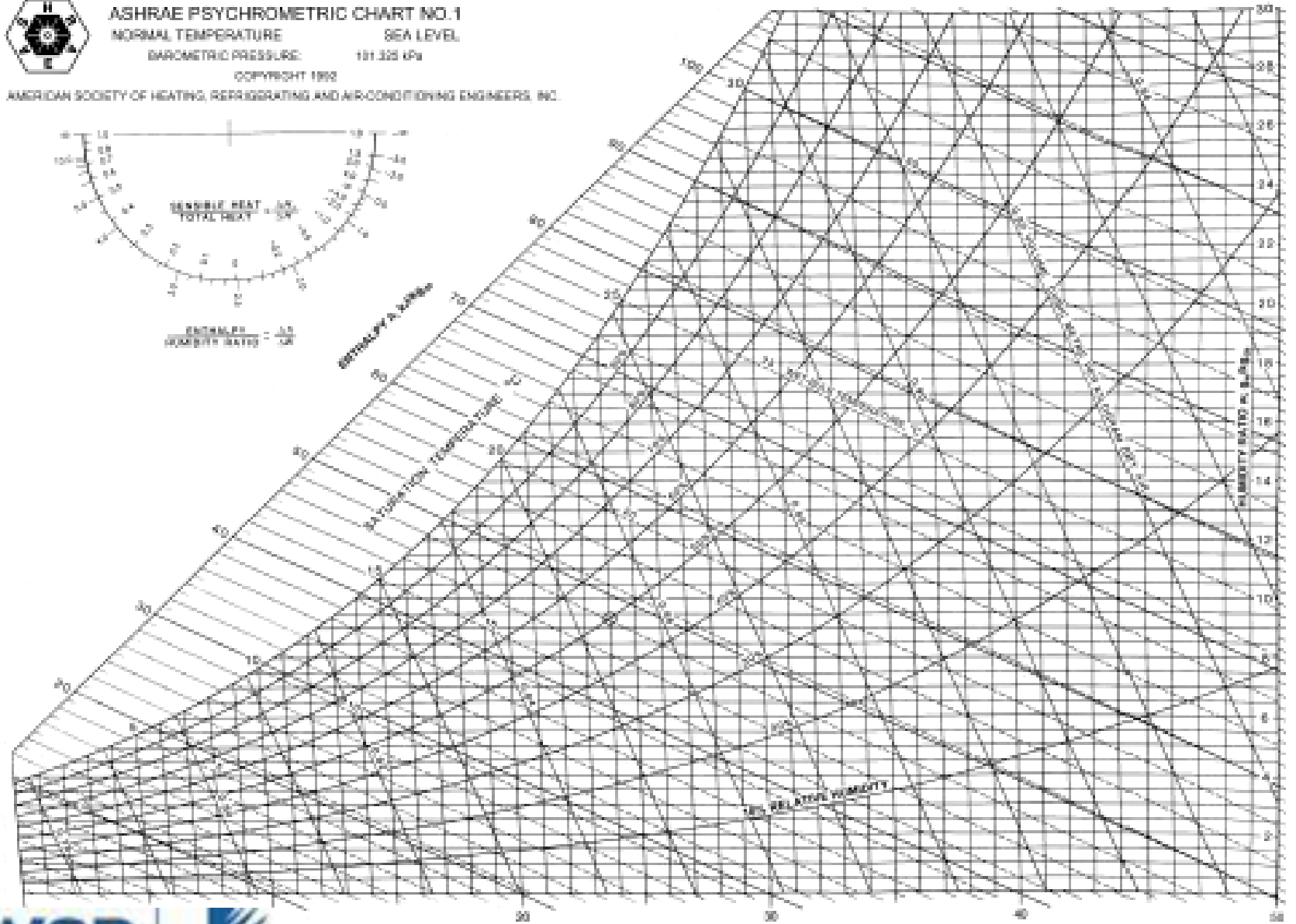
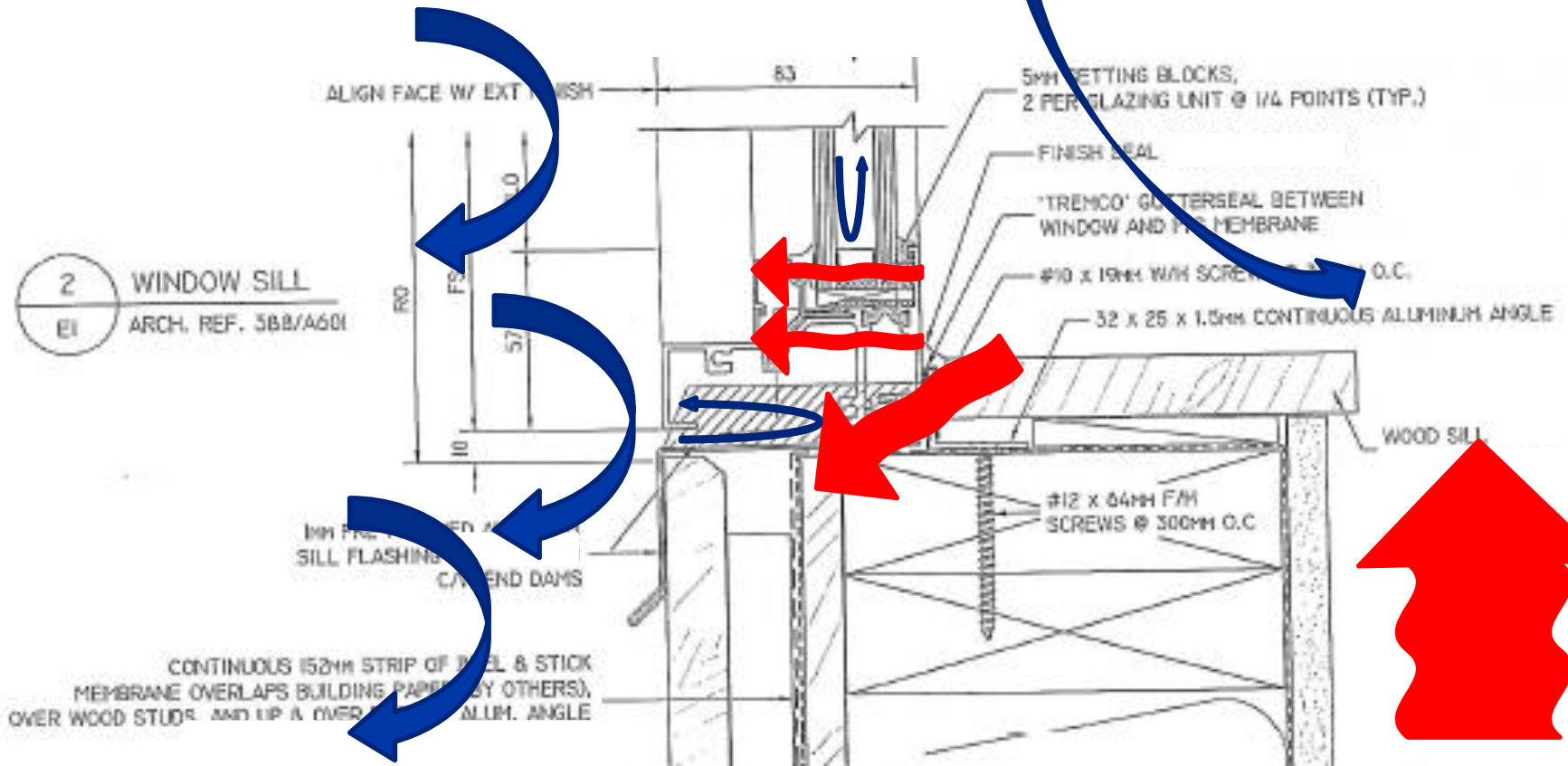
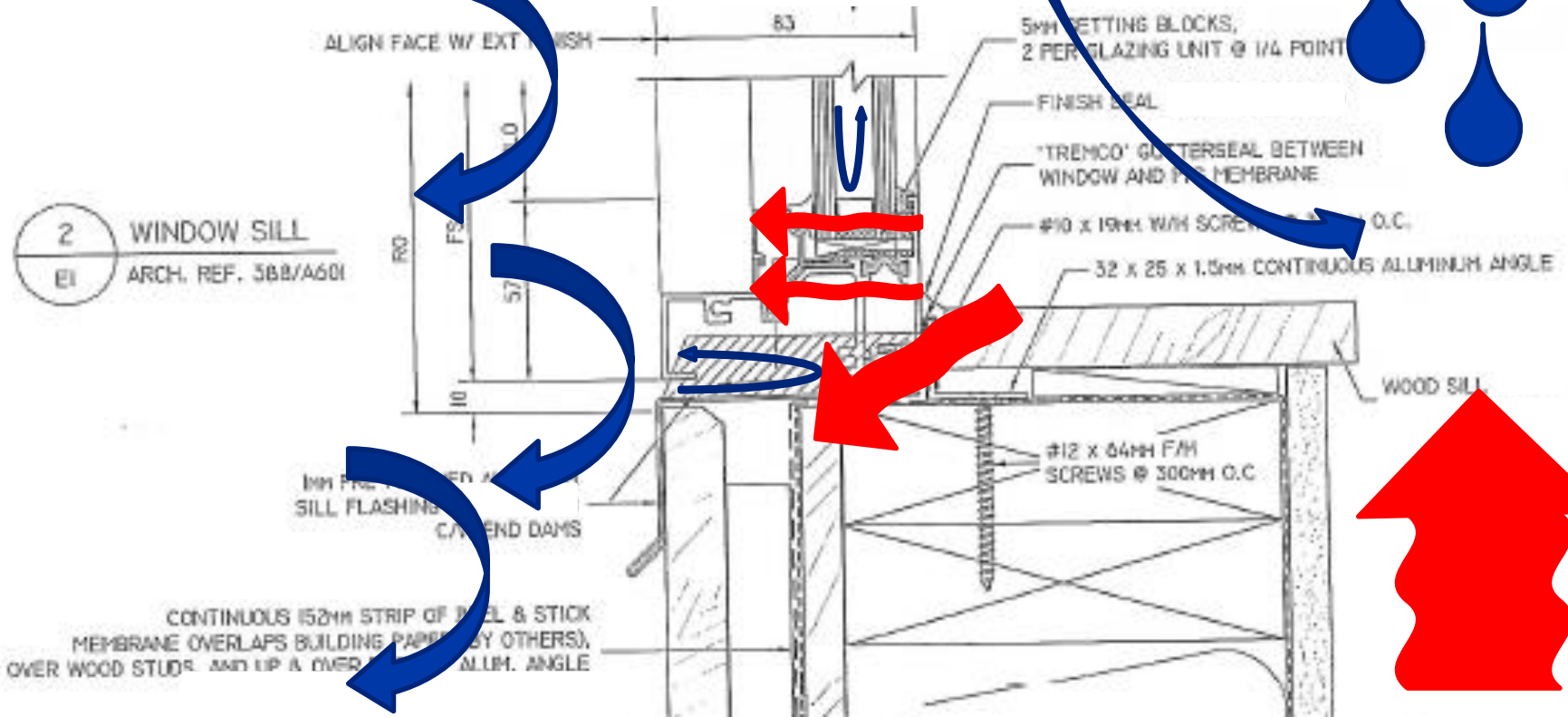


Fig. 1 ASHRAE Psychrometric Chart No. 1

Condensation on Windows



Condensation on Windows



The condensation resistance of fenestration systems is assessed by determining the product's Temperature Index (TI). TI is a non-dimensional parameter, which is defined as [3]:

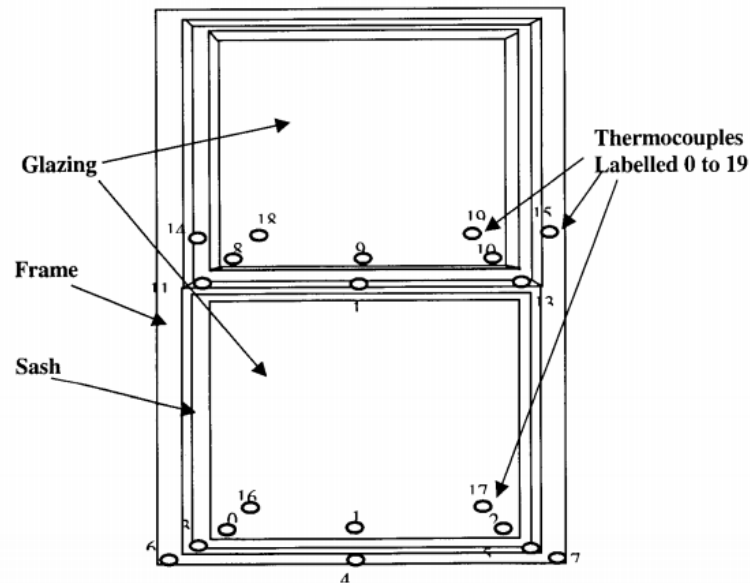
$$TI = \frac{T_{sp} - T_c}{T_h - T_c} \times 100 \quad (1)$$

where: T_{sp} specimen surface temperature, °C
 T_c weather (cold) side temperature, °C
 T_h warm (room) side temperature, °C

T_{sp} is measured at specific locations on the glass, frame and sash members of the product, as shown in Figure 1. T_h and T_c are measured at the main stream on the warm and cold side of the window, respectively.

T_h is maintained at $20 \pm 1^\circ\text{C}$, where as T_c is kept at $-18 \pm 1^\circ\text{C}$. The film heat transfer coefficients were kept at $8 \pm 1 \text{ W}/(\text{m}^2 \cdot \text{K})$ on the warm side (natural convection) and at $30 \pm 2 \text{ W}/(\text{m}^2 \cdot \text{K})$ on the cold side. More details about the test procedure, sample mounting, data reduction and other specifics can be found in Reference 1.

The Temperature Index is determined for the glazing, frame and sash members of the unit, and lowest value is used to "rate" the window for condensation resistance.



The final CR_c shall be calculated by area weighting these non-dimensional numbers for the center-of-glazing, divider, and edge-of-divider areas as given in Equation 4-2.

$$CR_c = \left\{ 1 - \left\{ \frac{\sum_k SS_{d_k} A_{d_k} + \sum_k SS_{deog_k} A_{deog_k} + \sum_k SS_{cog_k} A_{cog_k}}{\sum_k A_{d_k} + \sum_k A_{deog_k} + \sum_k A_{cog_k}} \right\}^{1/3} \right\} \times 100$$

Equation 4-2

*k=*center-of-glazing, divider, edge-of-divider sections, respectively

Where for each frame cross-section, k:

$$SS_{d_k} = \frac{\sum_j (S_d)_{j=RH @ 30\%, 50\%, 70\%}}{3}$$

$$SS_{deog_k} = \frac{\sum_j (S_{deog})_{j=RH @ 30\%, 50\%, 70\%}}{3}$$

$$SS_{cog_k} = \frac{\sum_j (S_{cog})_{j=RH @ 30\%, 50\%, 70\%}}{2}$$



SILL

ISO1 UNDO

TEMPERATURES

10.9

Celsius

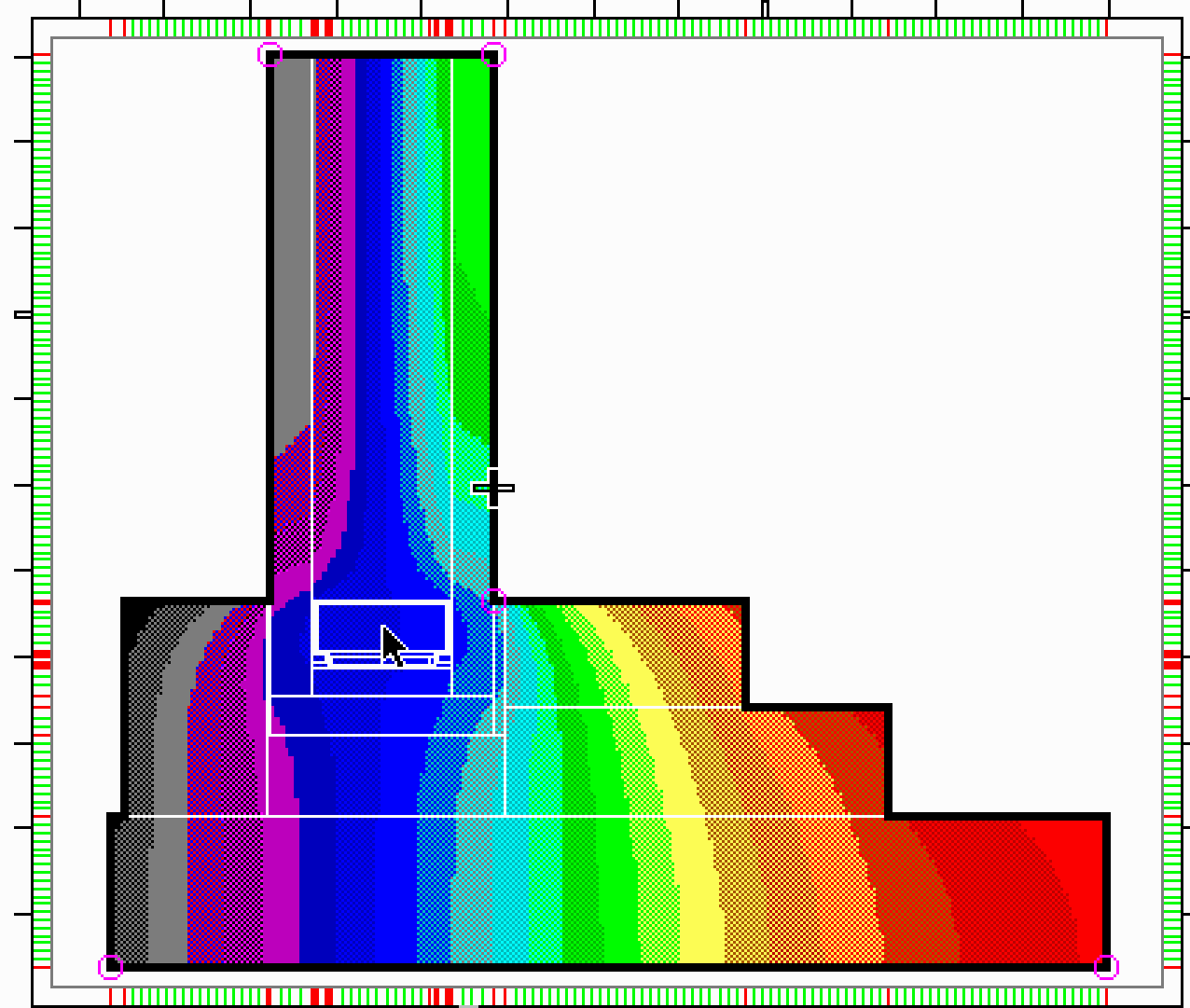
- 0.0
- 0.9
- 1.7
- 2.6
- 3.5
- 4.4
- 5.2
- 6.1
- 7.0
- 7.8
- 8.7
- 9.6
- 10.4
- 11.3
- 12.2
- 13.1
- 13.9
- 14.8
- 15.7
- 16.5
- 17.4
- 18.3
- 19.1
- 20.0

-31.750 | X
-20.320 | Y

MM

1.000:Step

** NO TITLE **



[10.00 MILLIMETERS BETWEEN TICKS]



SILL

ISO1 UNDO

TEMPERATURES

7.5

Celsius

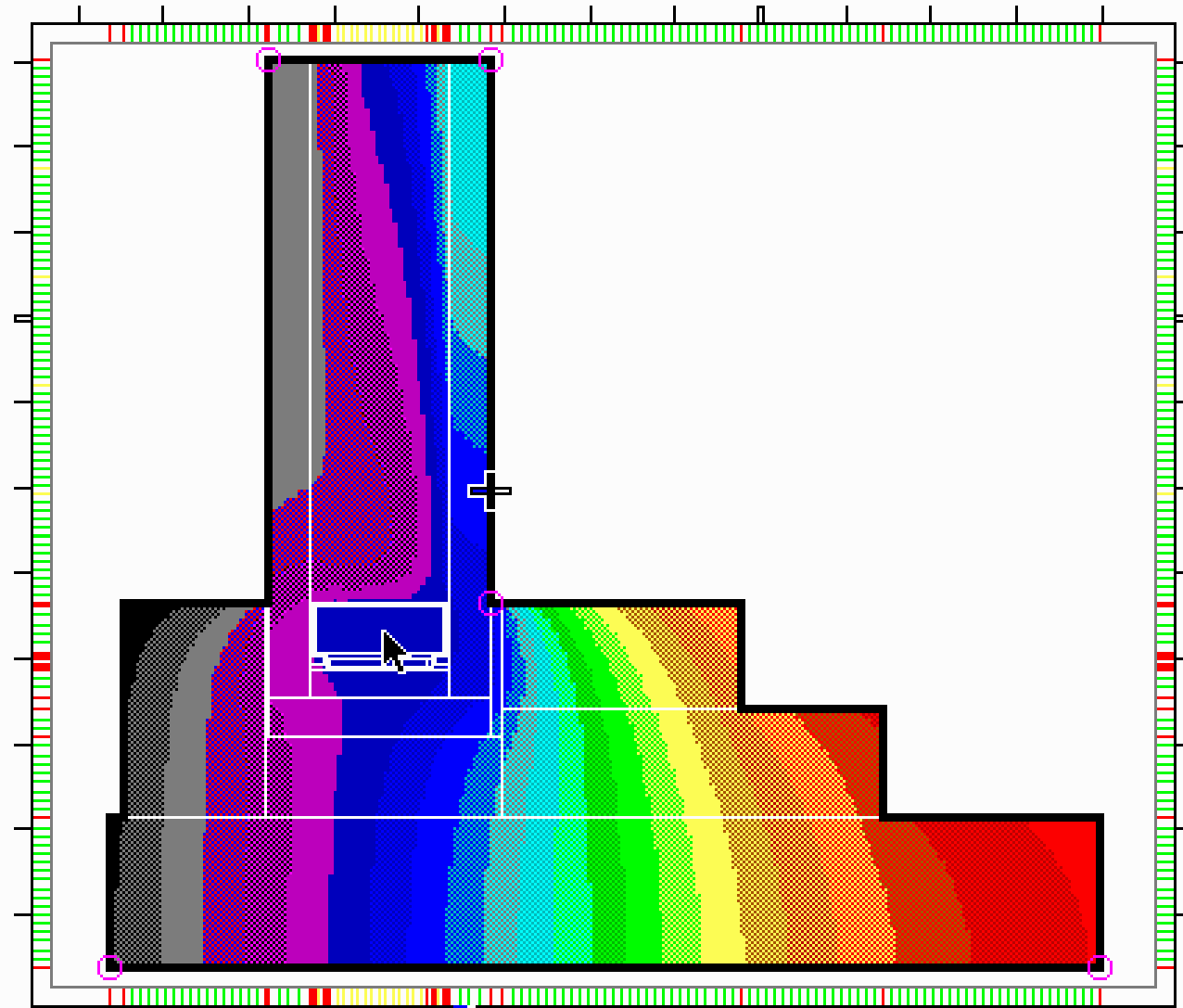
- 0.0
- 0.9
- 1.7
- 2.6
- 3.5
- 4.4
- 5.2
- 6.1
- 7.0
- 7.8
- 8.7
- 9.6
- 10.4
- 11.3
- 12.2
- 13.1
- 13.9
- 14.8
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- 16.5
- 17.4
- 18.3
- 19.1
- 20.0

-31.750 | X
-20.320 | Y

MM

1.000: Step

** NO TITLE **



[10.00 MILLIMETERS BETWEEN TICKS]





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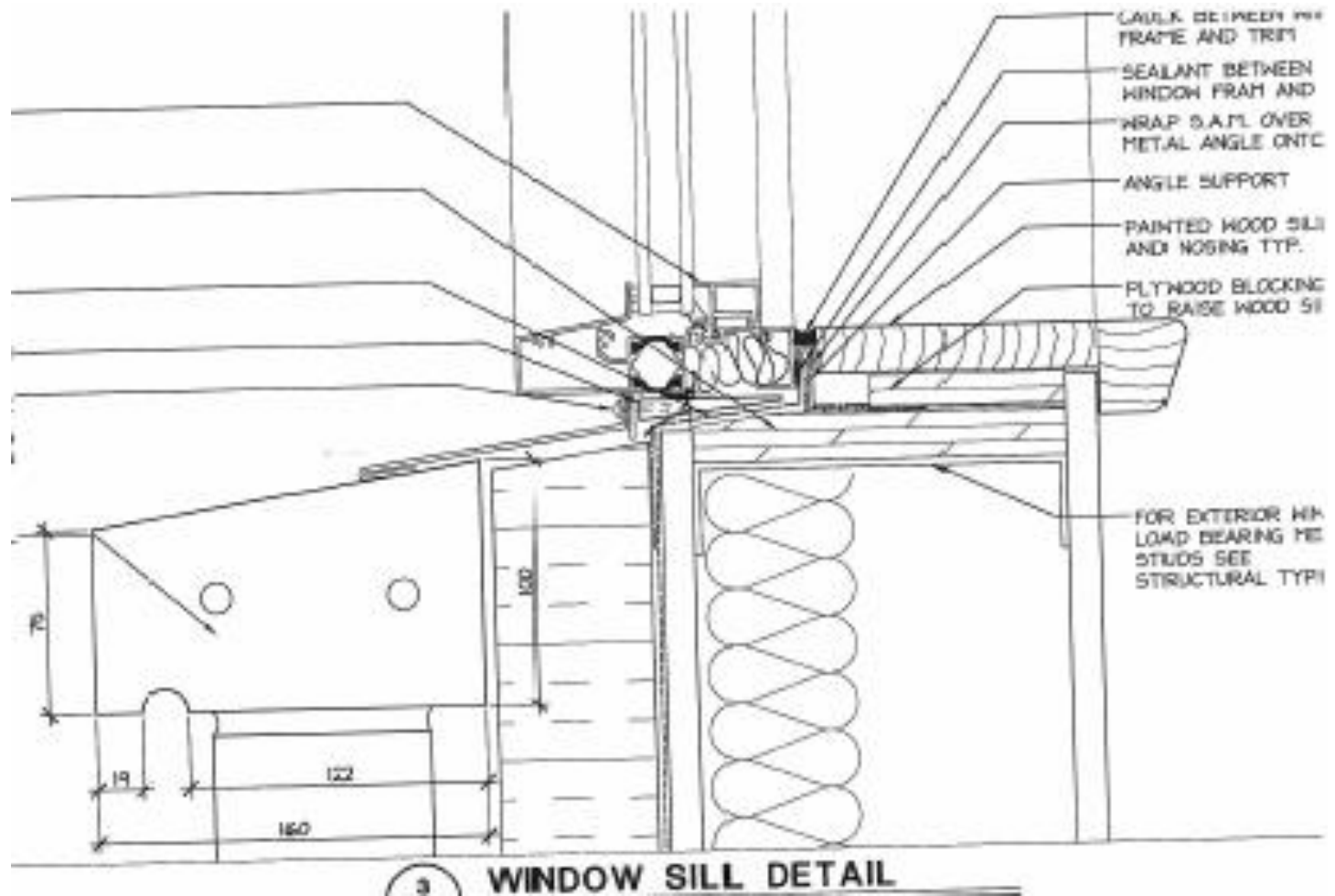
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Case Study #1



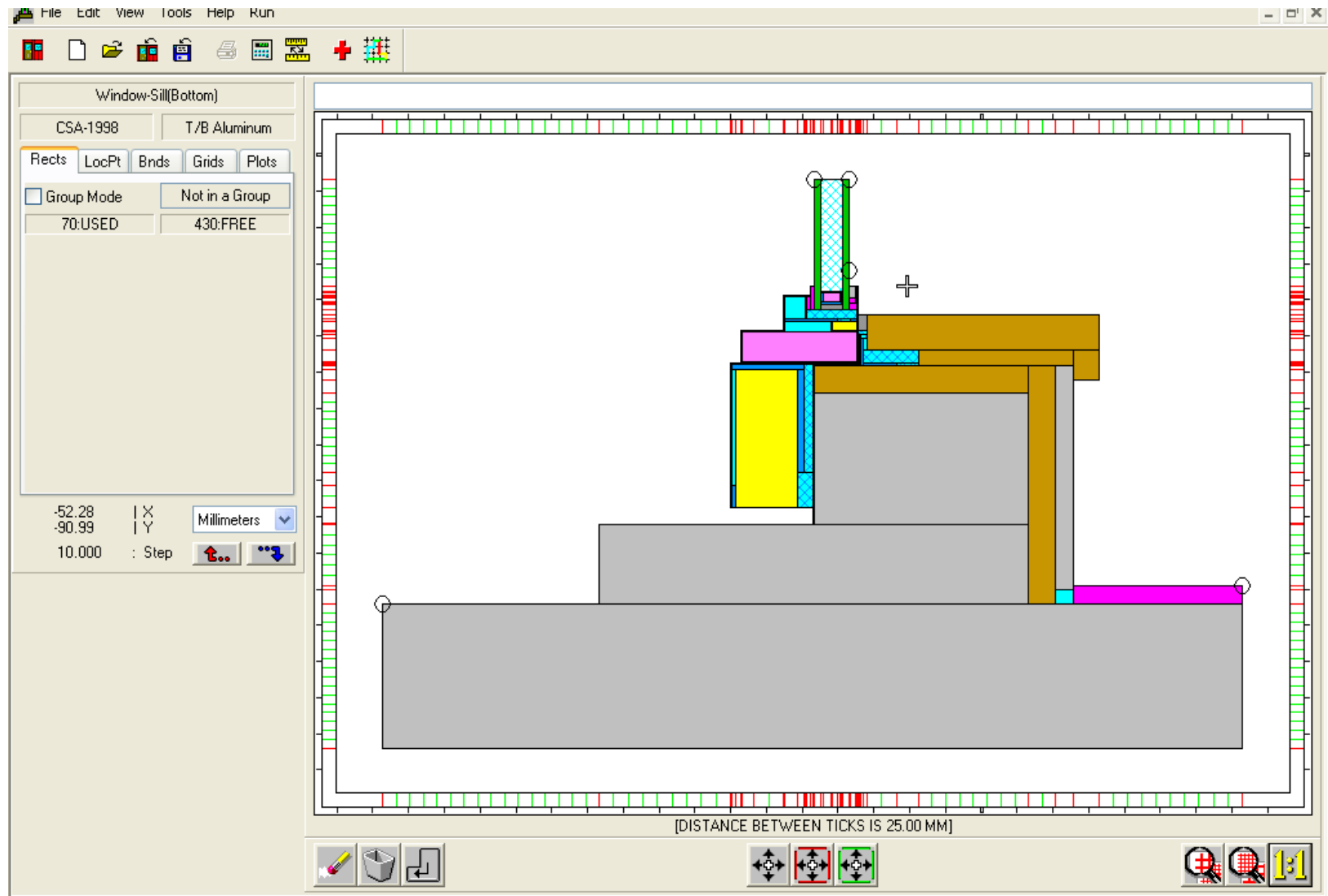
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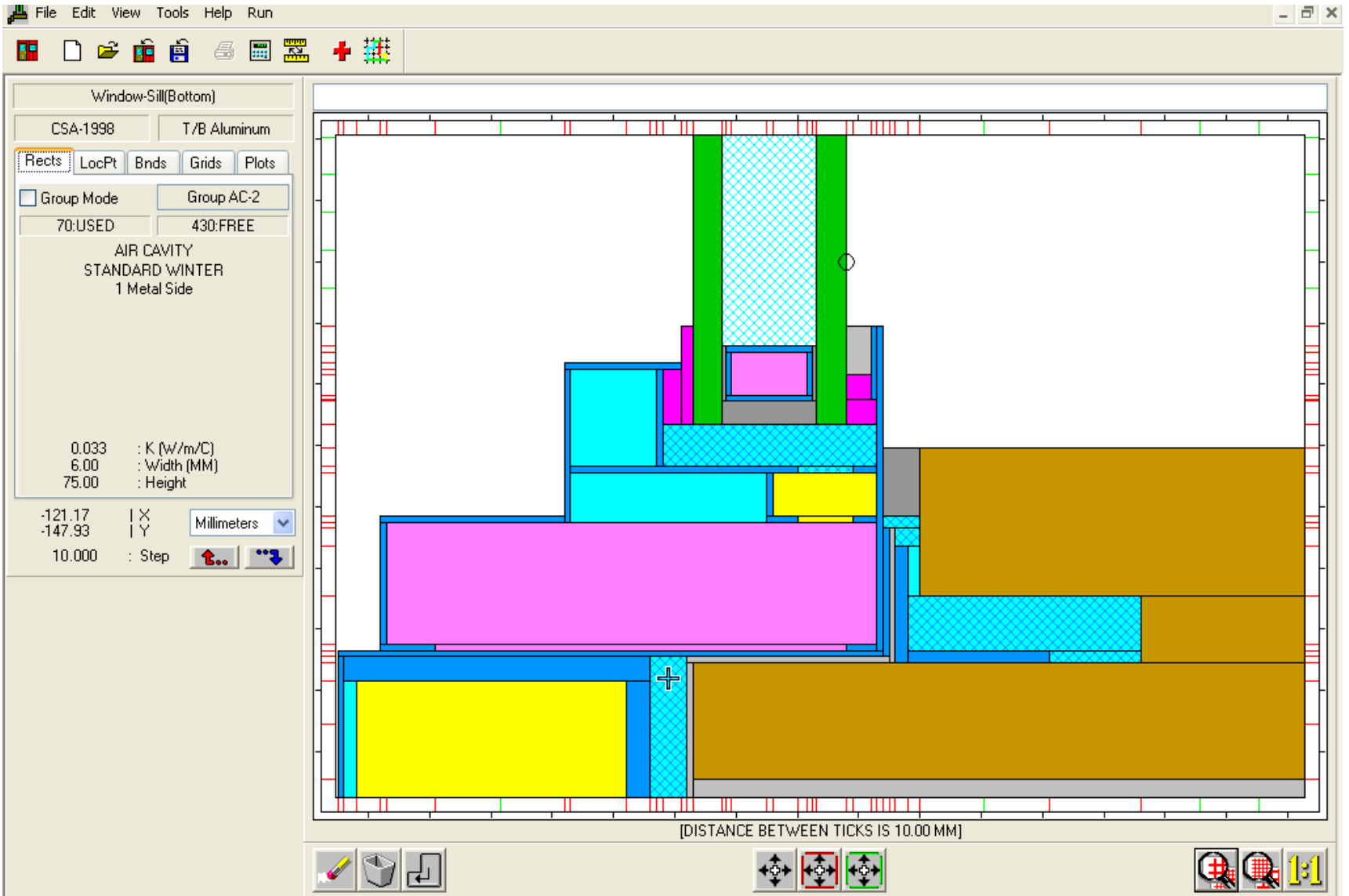
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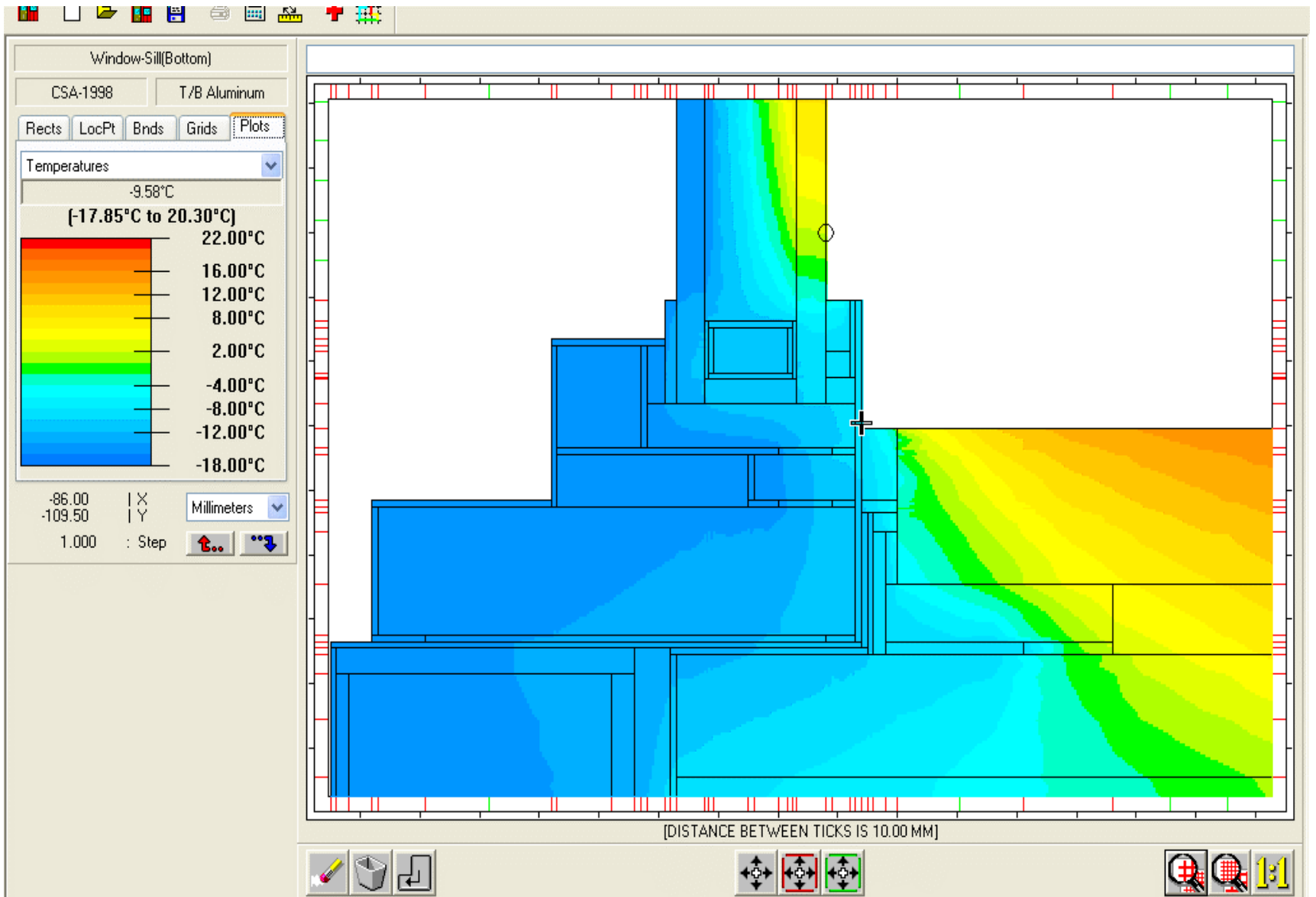
Go to section for review of new methods and press ENTER

100%



Go to position for corner of new rectangle and press ENTER

DFC



File Edit View Tools Help Run

CSA-1998 T/B Aluminum

Recls LocPt Bnds Grids Plots

Group Mode Group AC-2

84:USED 416:FREE

AIR CAVITY
STANDARD WINTER
1 Metal Side

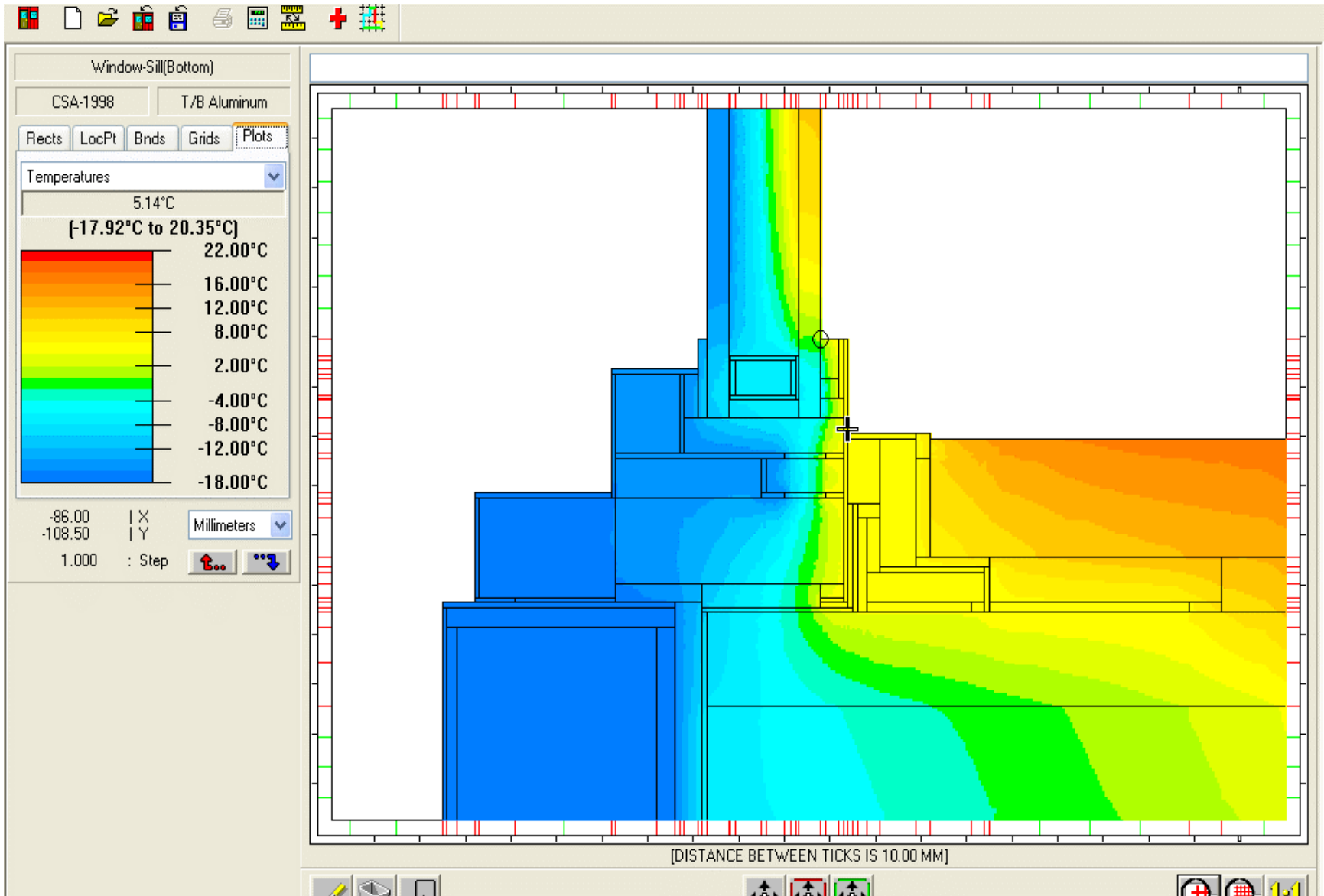
0.033 : K (W/m/C)
6.00 : Width (MM)
76.00 : Height

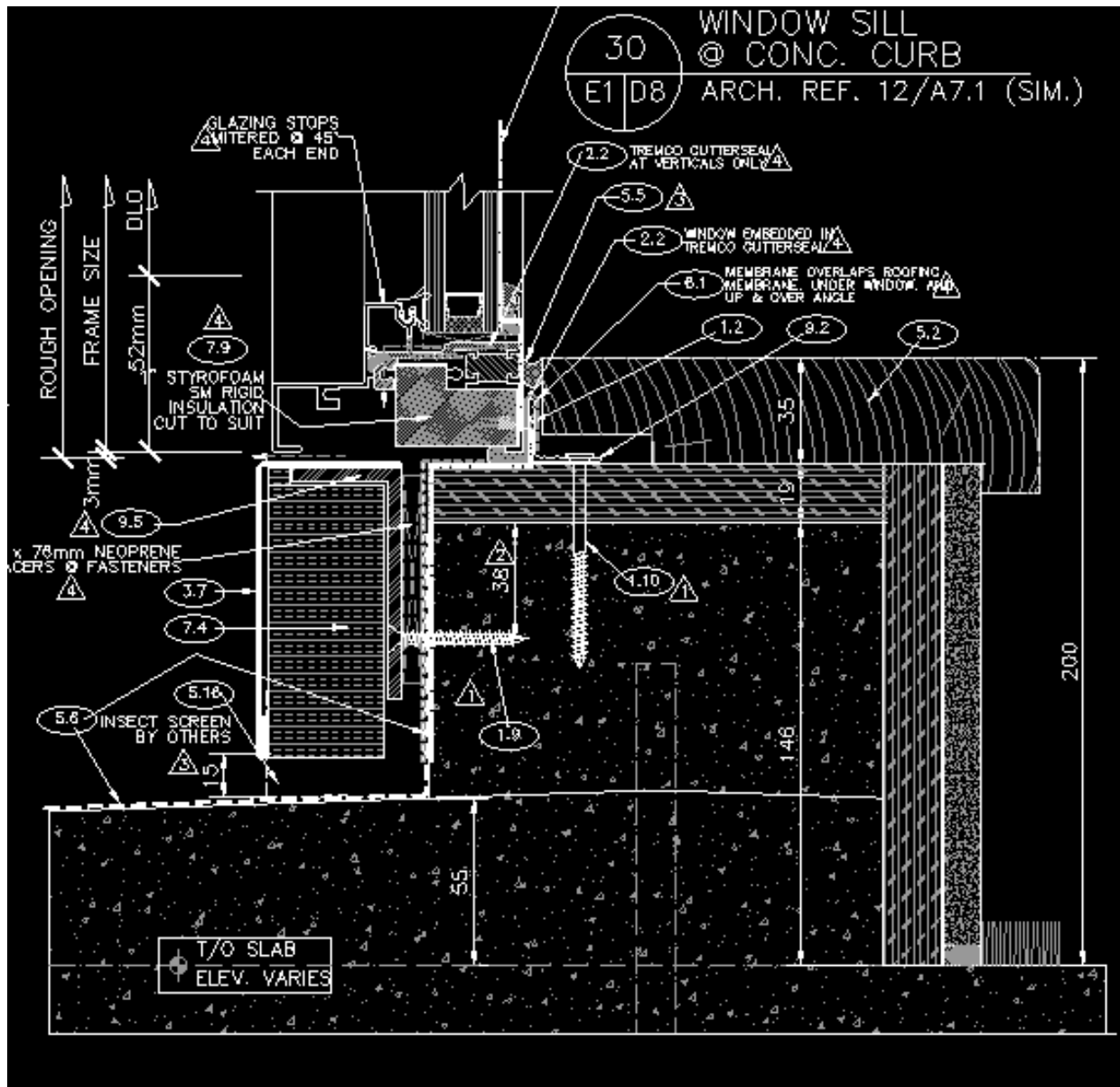
-121.07 | X
-146.43 | Y Millimeters
10.000 : Step

[DISTANCE BETWEEN TICKS IS 10.00 MM]

Go to position for corner of new rectangle and press ENTER

DFC





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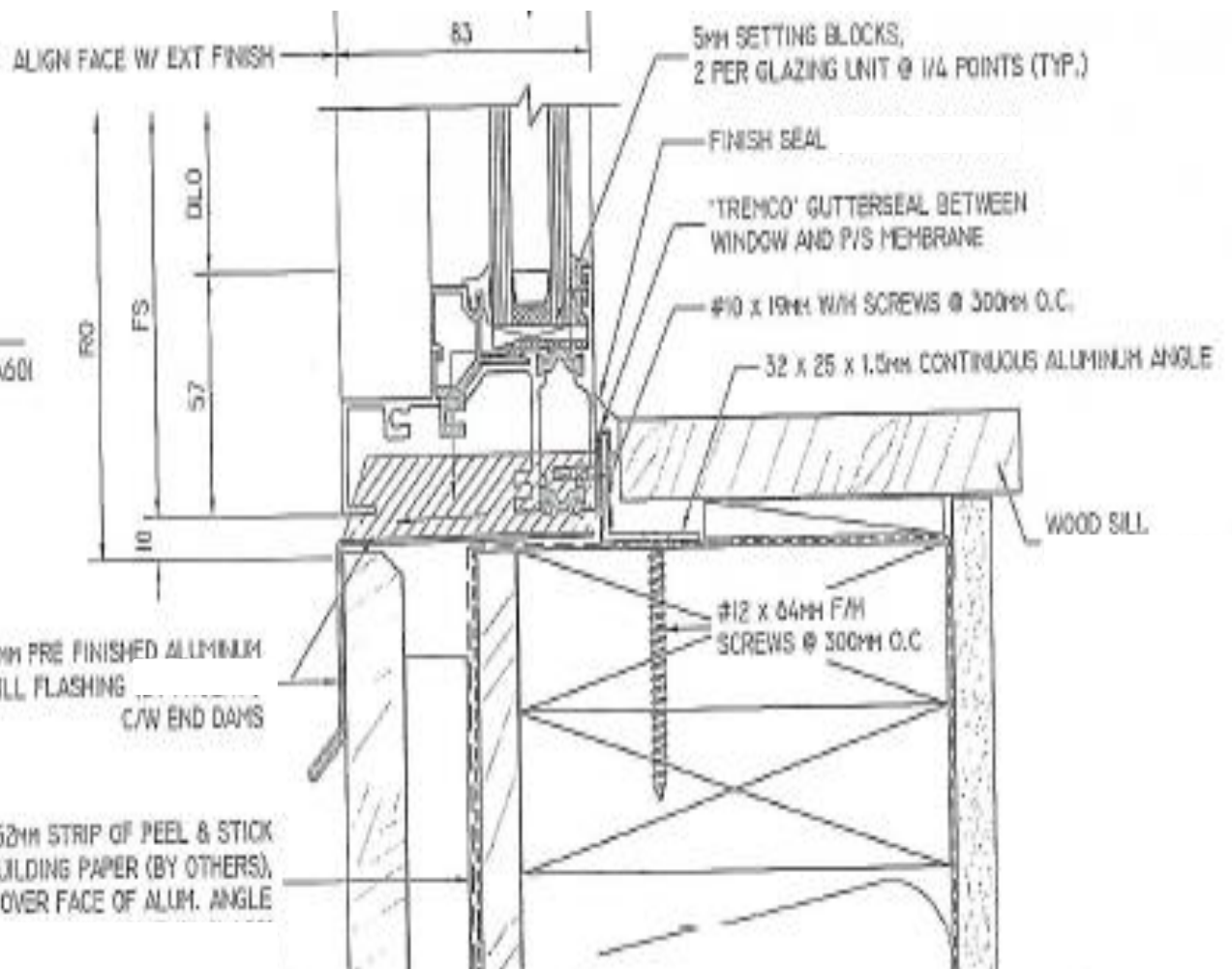
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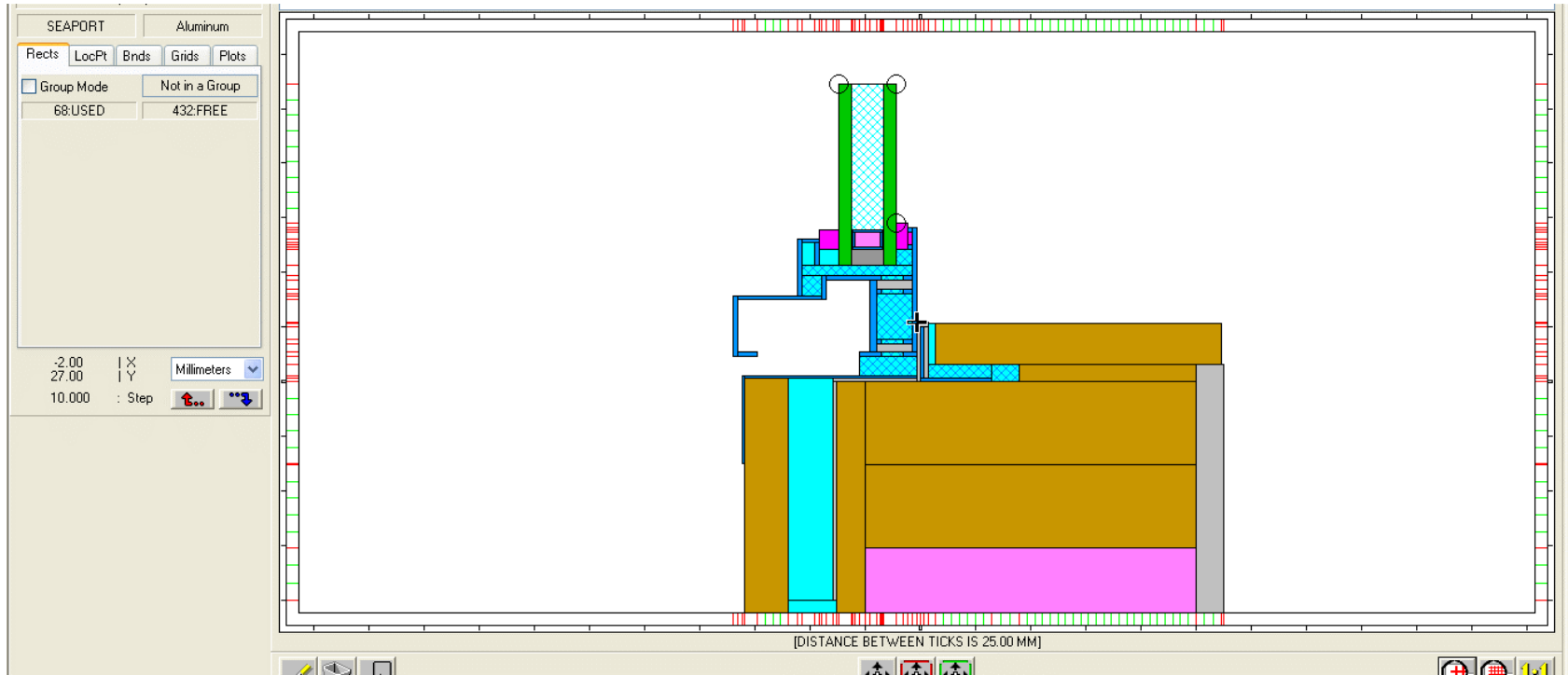
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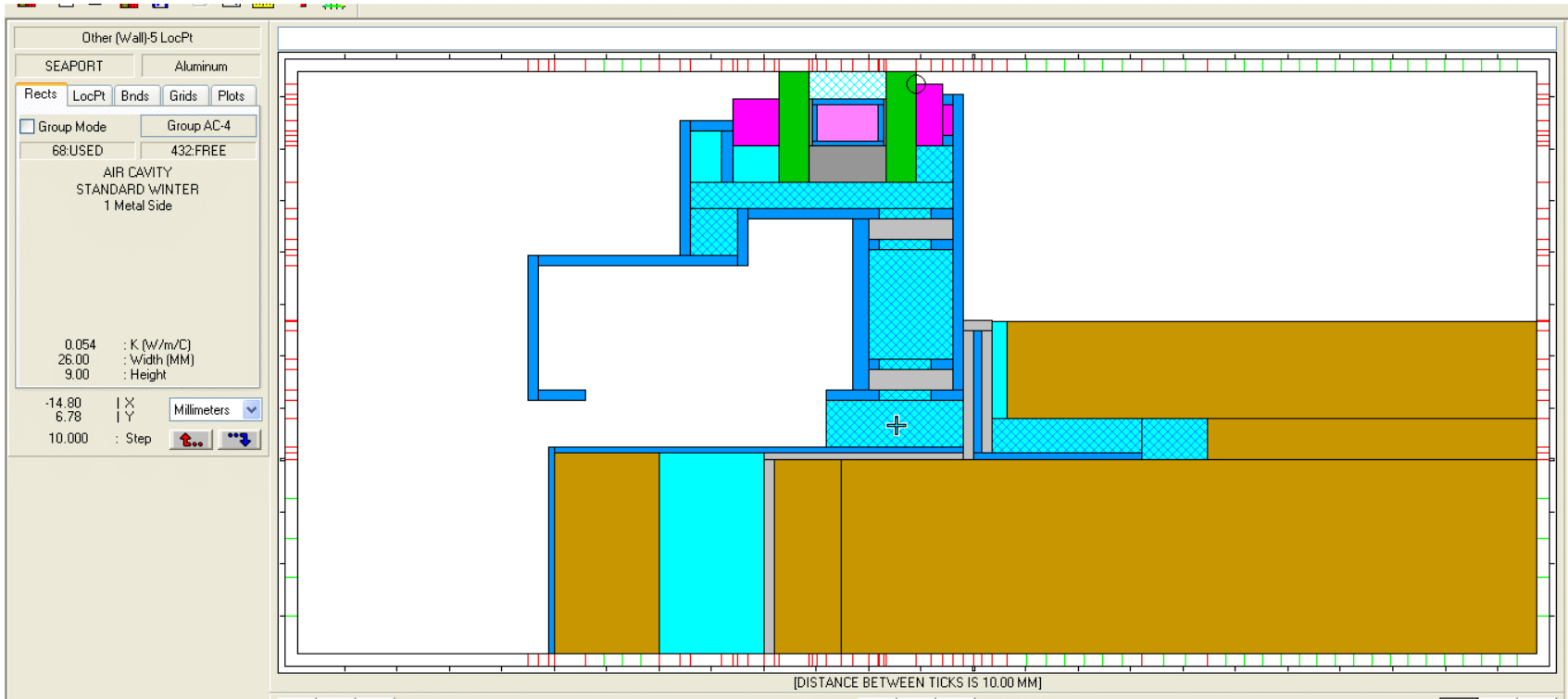
Outline of Presentation

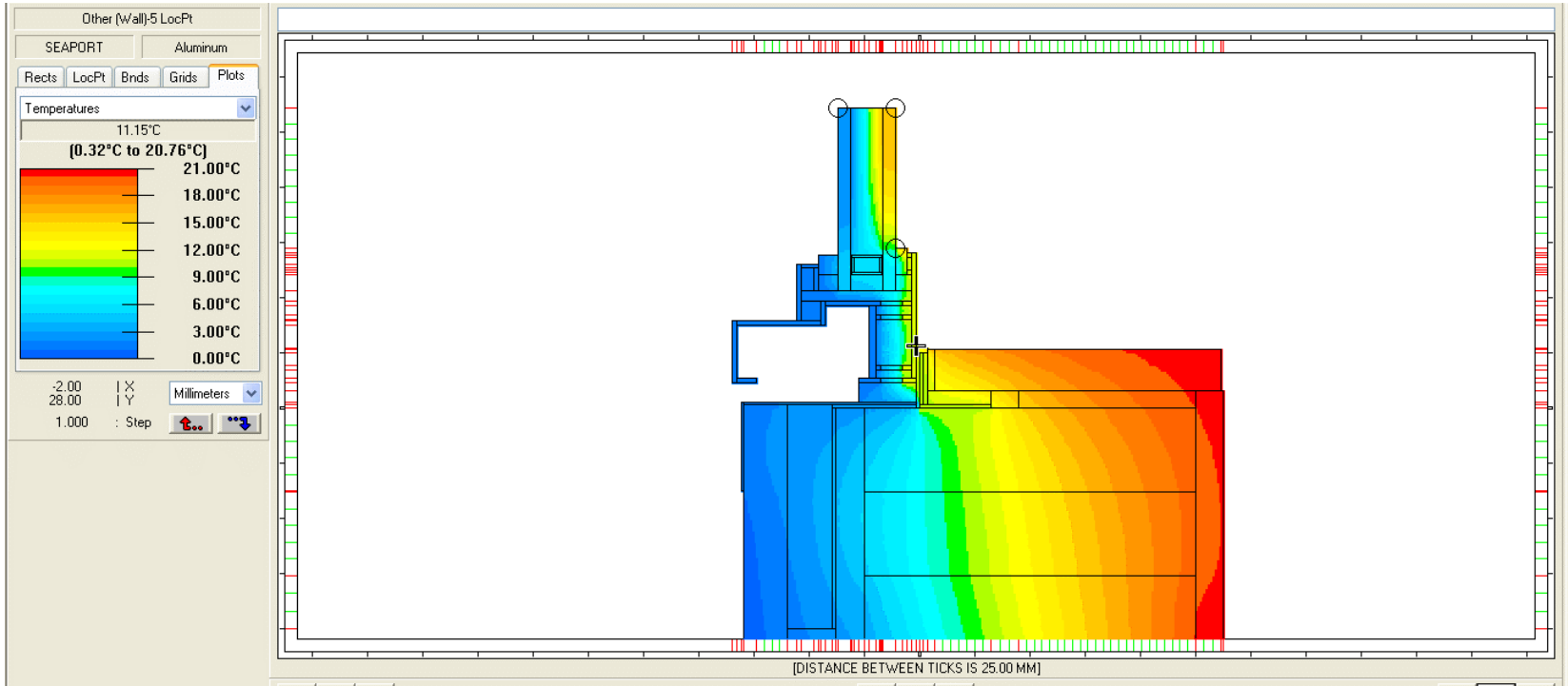
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2 WINDOW SILL
 EI ARCH. REF. 388/A601



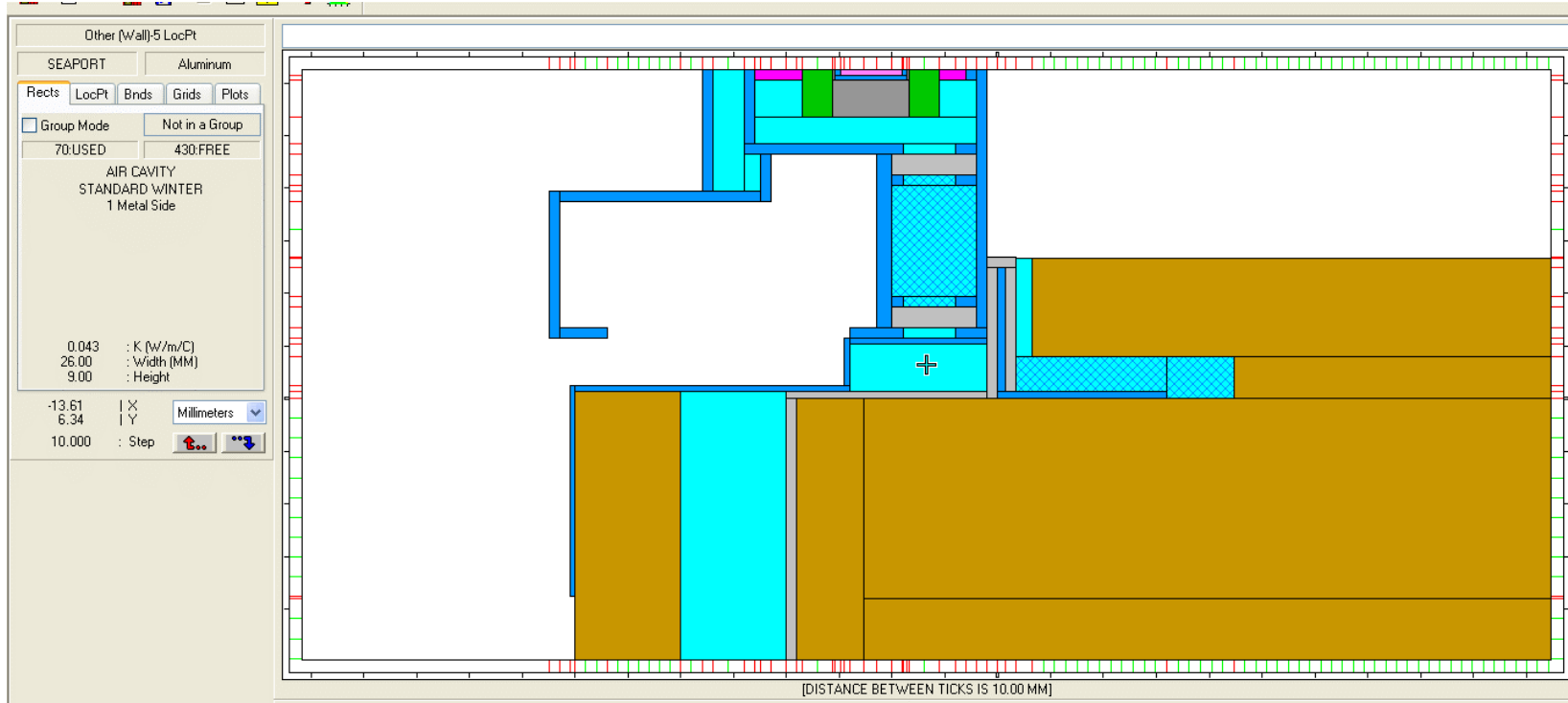


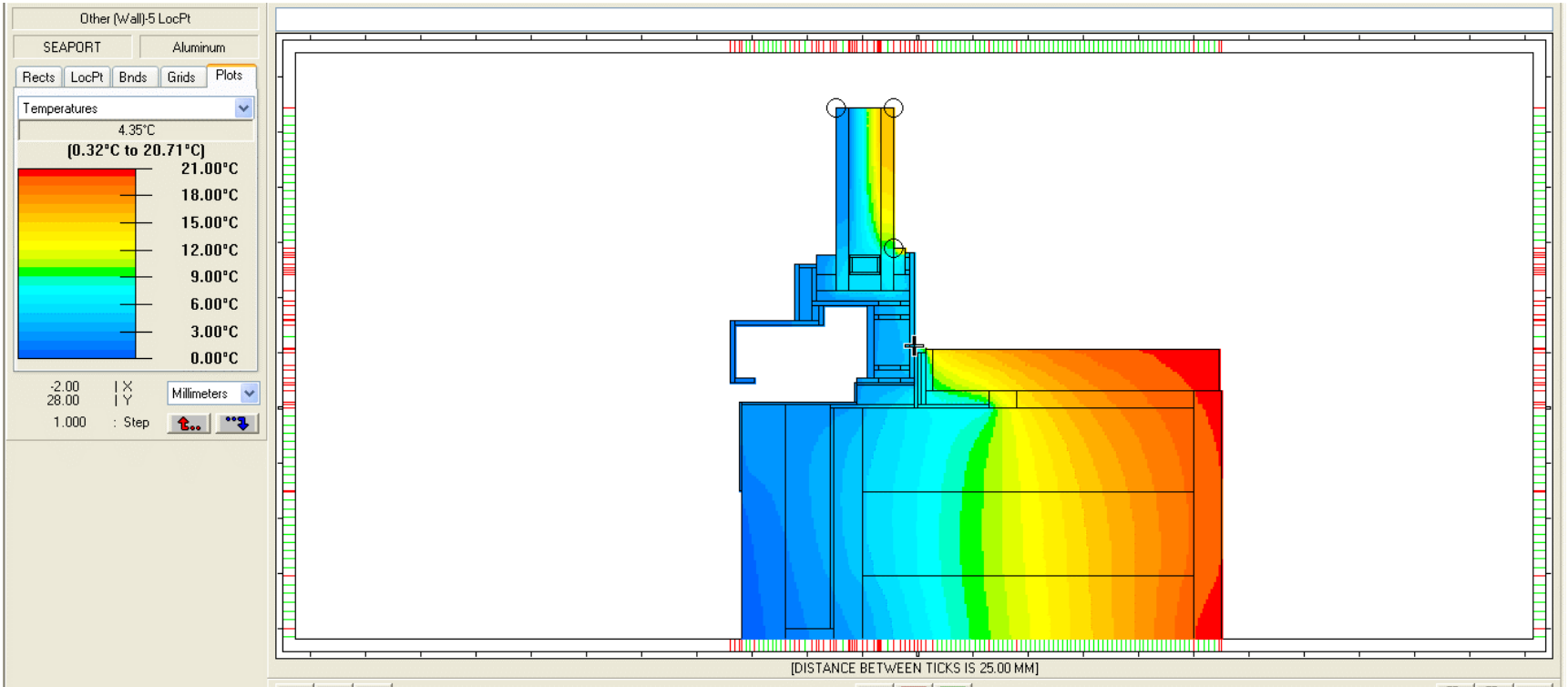


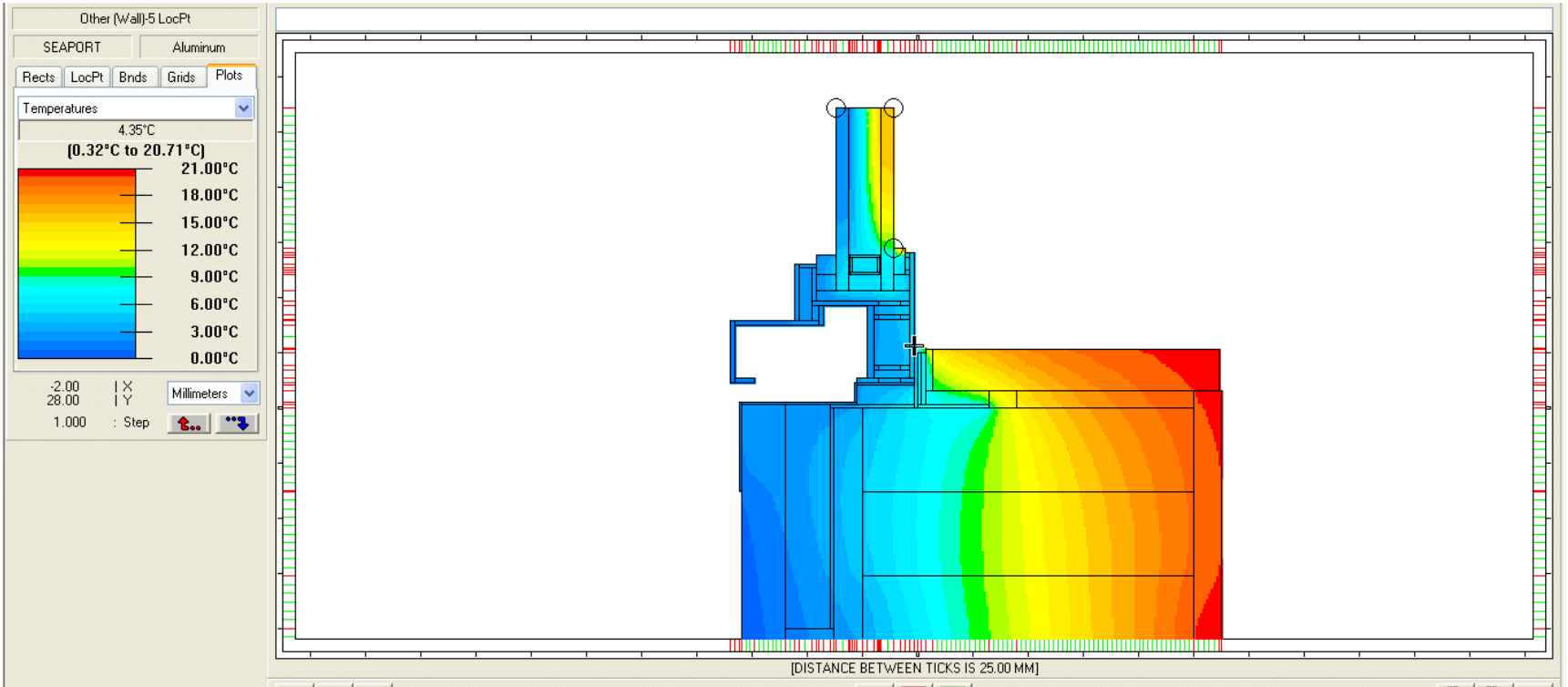


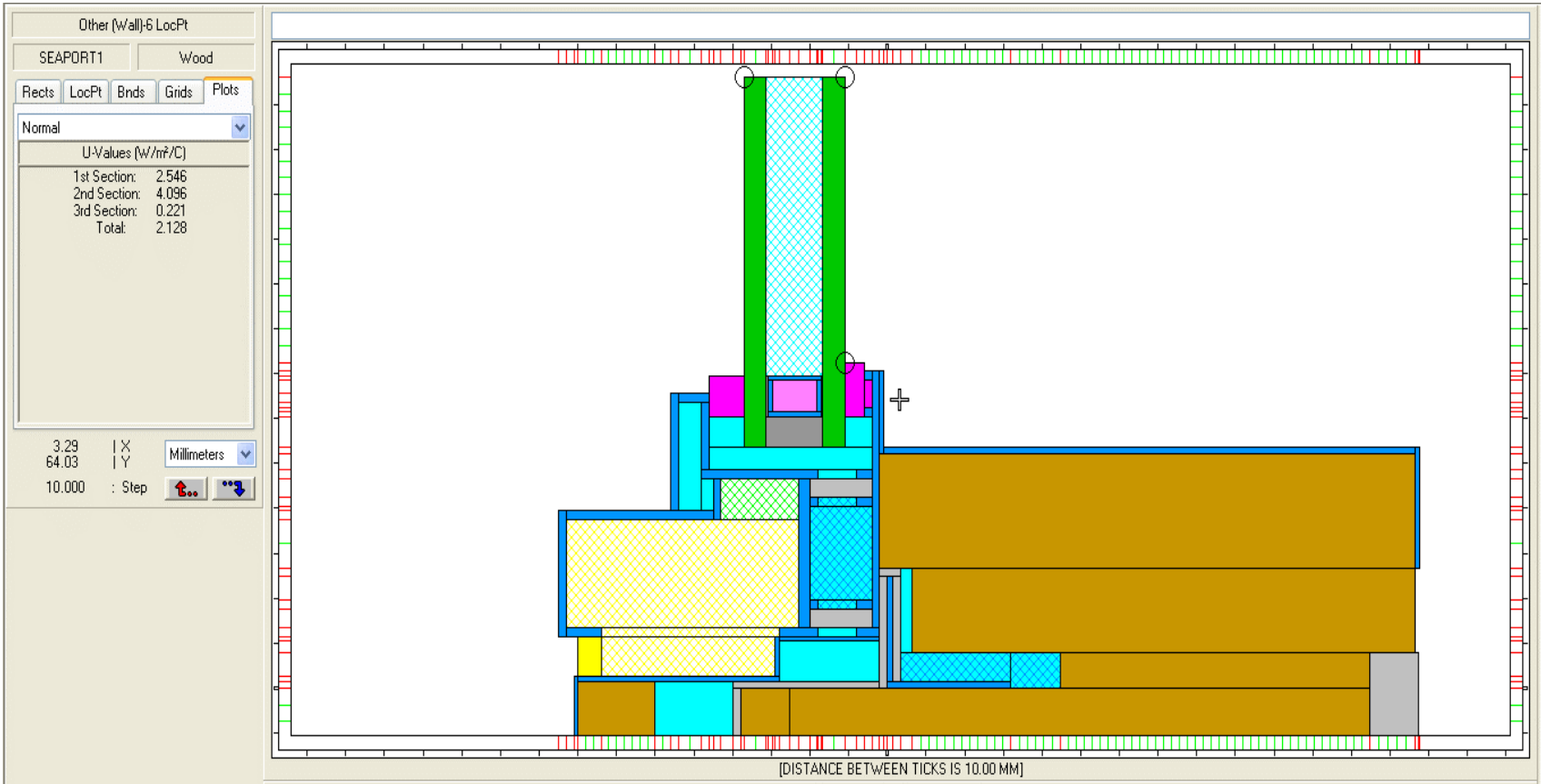












Option	Configuration	Sill Temperature	Difference from base case
0	Base case (as discovered)	12.0 °C	-
1	Remove backleg of sill flashing, reduce thermal bridge	12.1	0.1 °C
2	Lower interior sill liner to expose sill frame	12.4	0.4
3	Close in exterior cavity to reduce wind-washing (+ Option 2)	13.4	1.4
4	Separate sill flashing from frame (+ Option 2)	16.3	4.3
5	Separate sill flashing from frame (+ Options 2 and 3)	16.6	4.6
6	Remove sill flashing from interior frame (+ Option 2)	17.4	5.4
7	Remove sill flashing from interior frame (+ Options 2 and 3)	17.6	5.6
8	Heat sink on the horizontal face of the sill liner	15.5	3.5
9	Heat sink on horizontal and vertical faces of the sill liner	15.8	3.8
10	Base case, but with interior blinds closed	10.6	-1.4











Time of measurement	Room air temperature	Relative humidity	Dew-point Temperature
09:35	23 °C	73%	17.8 °C
10:20	22 °C	64%	15.2 °C
10:40	21.5 °C	61%	13.5 °C





ASHRAE PSYCHROMETRIC CHART NO. 1

NORMAL TEMPERATURE SEA LEVEL

BAROMETRIC PRESSURE: 101.325 kPa

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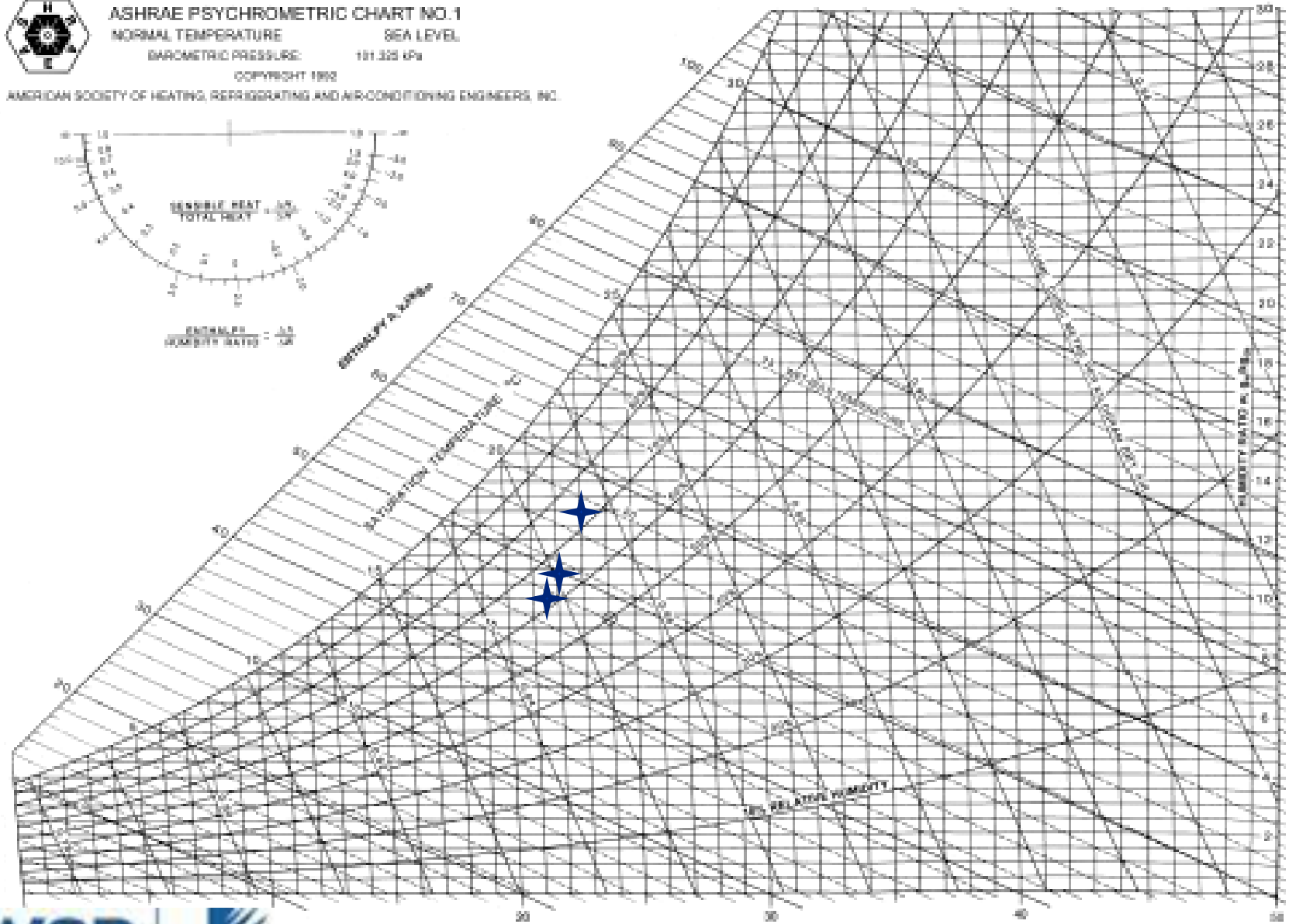
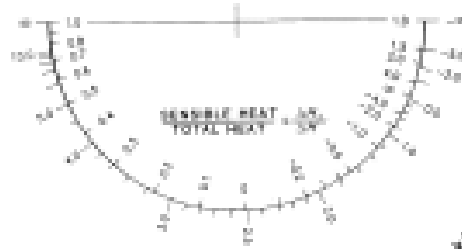


Fig. 1 ASHRAE Psychrometric Chart No. 1

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$$Q = E F A \sigma (T_h^4 - T_c^4)$$

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Questions?