

CONDENSATION ANALYSIS IN A COLD CLIMATE

Wesley Narciso, P.Eng., CRP, PRA, LEED AP

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OUTLINE

- History and Background
- Visual Review
- Testing Methodology
- Results and Discussion
 - Psychrometric and Thermal Analysis
 - Ventilation Conditions (ASHRAE, Thermal Comfort and CONTAM Modeling)
- Conclusion
- Recommendations





Property and Climate info

Location: Whistler, BC (between Highway 99 and Whistler/Blackcomb Mountains)

Construction Date: Circa 1999

Management Structure: Stratified property with private hotel management and original developer on strata council

Whistler:Vancouver (YVR):Temps (Nov to Feb): -3.2°C to 0.6°CTemps (Nov to Feb): 3.3°C to 6°CDays under 0°C: 152 daysDays under 0°C: 46 days

*Environment Canada (Climate Services)



Building description:

- 1 building (2 towers), over 380,000 ft² (gross floor area)
- 10 stories, 419 units, 19 staff units
- Multiple amenities (restaurants, lounges, ballroom, conference rooms, spa, child care, business centre, commercial/retail units etc.) with strict and unpredictable occupancy limitations

Structure and Building Envelope:

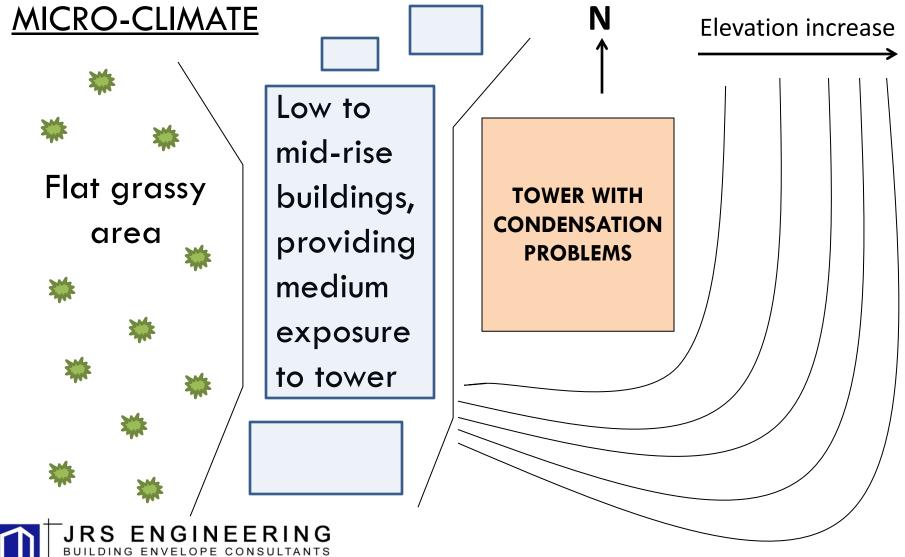
- Concrete tower with steel stud infill walls
- Exterior Insulated Finishing System (EIFS) with sloped metal shingle roof
- Aluminum framed, thermally broken glazing (window wall, punched windows and sliding doors)



Macro Climate

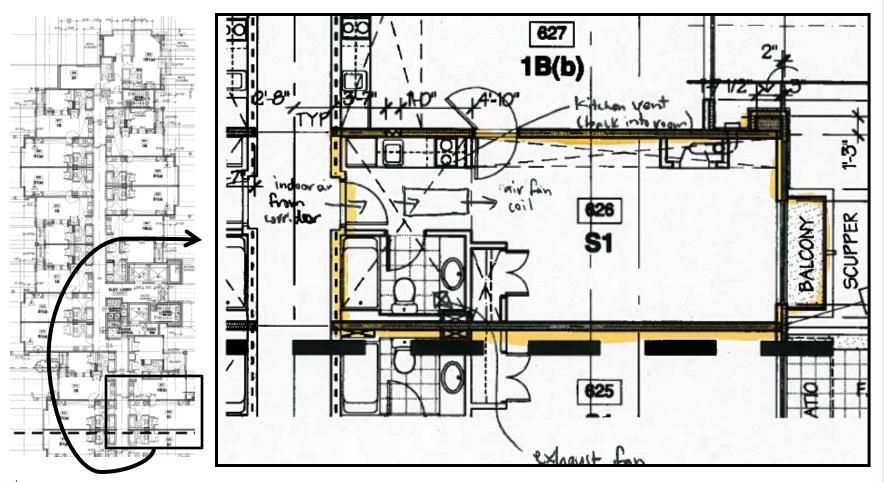






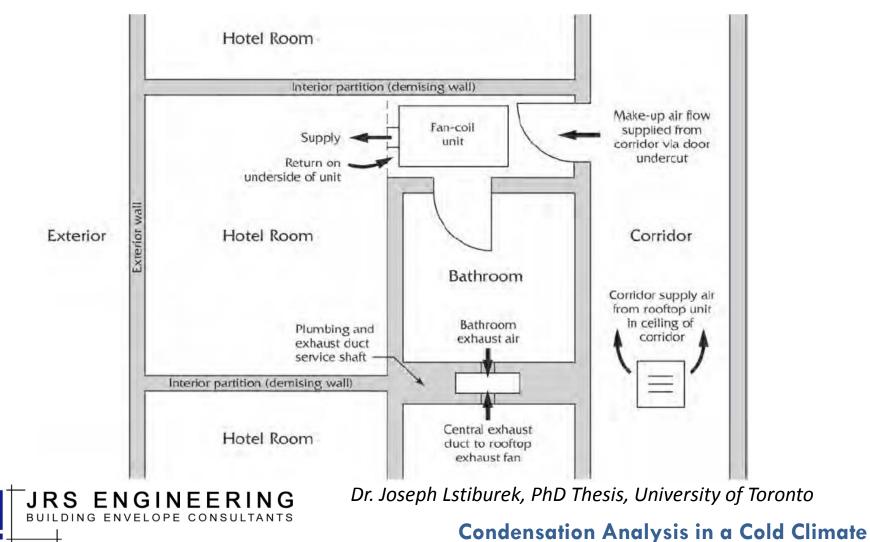


Floor Plan and Room Configuration

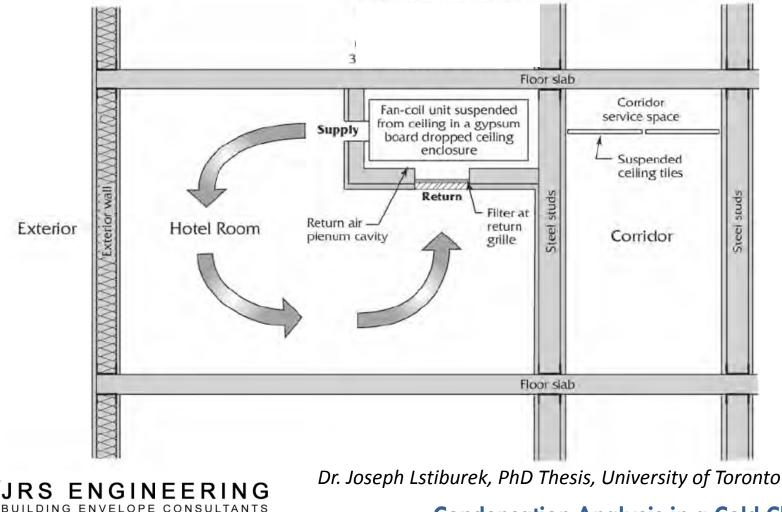


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Hotel Room/Bath Suite (Plan View)



Hotel Room/Bath Suite (Section View)





Corridor outside Rooftop air supply Rooftop Hotel HVAC System exhaust fan exhaust fan Bathroom -Bathroom exhaust exhaust Bathroom Bathroom exhaust exhaust Central exhaust entral exhaust supply duct Corridor air duct duct Bathroom - Bathroom exhaust exhaust Hotel Room/ Hotel Room/ Corridor **Bath Suite Bath Suite** Undercut

Dr. Joseph Lstiburek, PhD Thesis, University of Toronto

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TESTING METHODOLOGY

Air Temperature and Humidity Measurements (Interior and Exterior, High and Low)





TESTING METHODOLOGY

Surface Temperature Measurements (Interior and Exterior, High and Low)





Smoke Pencil Video



TESTING METHODOLOGY

Airflow rates (Under door, bathroom fan, FCU)







TESTING METHODOLOGY

Moisture Loaded Scenario





RESULTS AND DISCUSSION

Psychrometric Analysis of Sliding Door

- Dew point calculations
- Simplified conductance heat flow
- Heat flow modeling (THERM)

Ventilation Conditions

- ASHRAE calculations (Supply/Exhaust Air)
- FCUs and other fans
- Thermal comfort (Fanger Model)
- CONTAM modeling



Dew Point Calculations

	Average Temp	Average RH	Dew Point				
Location	(C)	(%)	Temp (C)				
FEBRUARY 10, 2014							
	Semi-Vacant						
Living Room/Kitchen (Air)	21	47	9.3				
Near Sliding Door (Air)	19	45	6.7				
Sliding Door Surface (Surface)	3						
	Moisture Loaded						
Living Room/Kitchen (Air)	25	82	21.4				
Near Sliding Door (Air)	23	67	16.6				
Sliding Door Surface (Surface)	9						
MARCH 29, 2014							
	Semi-Vacant						
Living Room/Kitchen (Air)	21	42	7.4				
Near Sliding Door (Air)	18	50	7.4				
Sliding Door Surface (Surface)	8.5						



Typical semi-vacant scenario (average conditions):

Temp: **21°C** & RH: **45** % Dew Point Temp: **8.7°C** To avoid condensation, the coolest surface in the room (sliding door frame) must be above **8.7°C**.

Air Leakage: Observed air leakage with use of smoke pencil at joints in the frame. This air leakage reduces the interior surface temperature of frame due to wind washing.

Convection: Heating fan coil intended to provide air circulation at sliding door. Heavy floor to ceiling curtains impeded the convection currents.



Conductance Heat Flow (Current door vs. New Door)

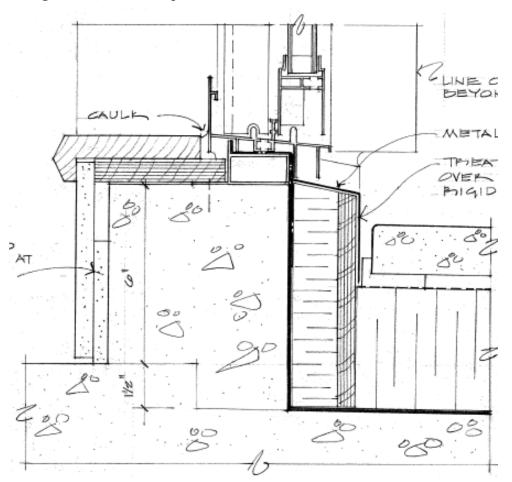
 $\mathbf{Q} = \mathbf{Area} \times \mathbf{U} \cdot \mathbf{Value} \times (\mathbf{T}_{\text{Inside}} - \mathbf{T}_{\text{Outside}}) \qquad (\text{Watts})$

Interior surface of existing door (U-value of 2.8 W/m²°C) = 3°C Interior surface of a new, better insulated door (e.g. 1.6 W/m²°C) = 9.5°C *Assuming constant area and heat flow

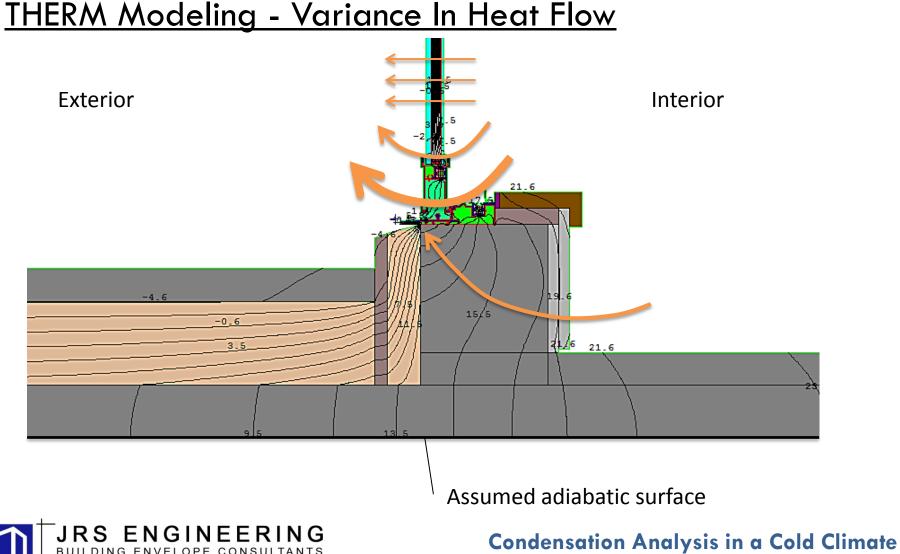
Interior surface temp **9.5°C > 8.7°C** (Dew point temp). Therefore, less likely to condense on new slider.



THERM Modeling – Set up

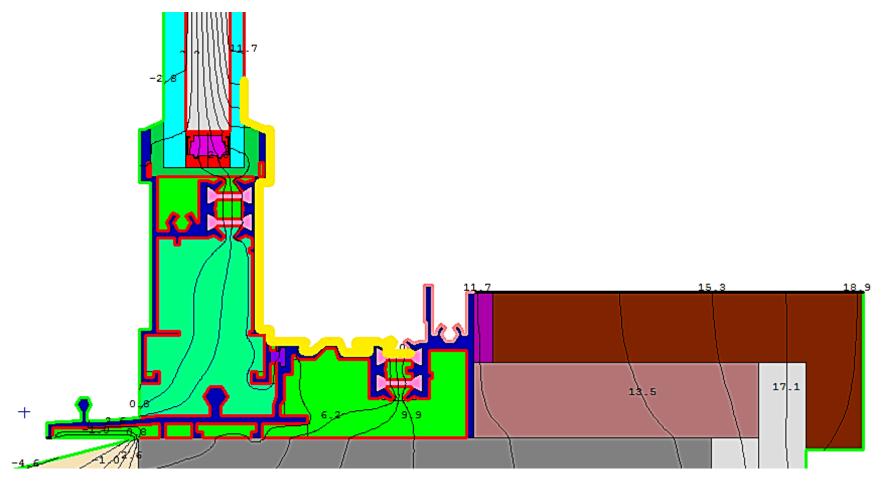






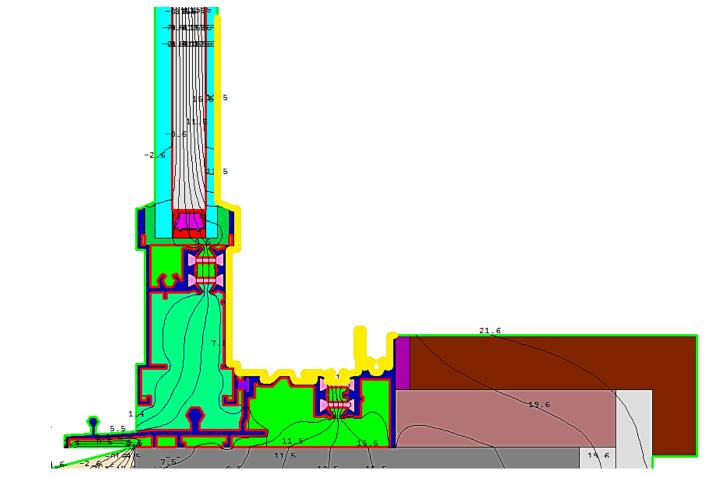
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THERM Modeling – Condensation Potential (Semi-Vacant)



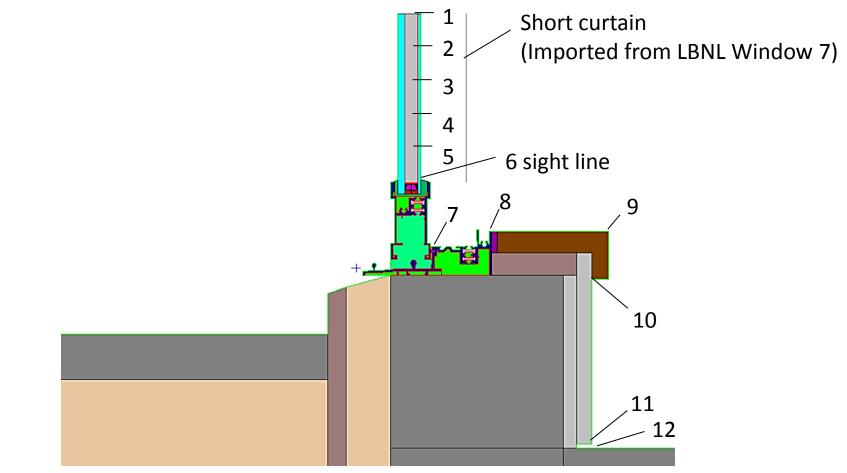


THERM Modeling - Condensation Potential (Moisture Loaded)



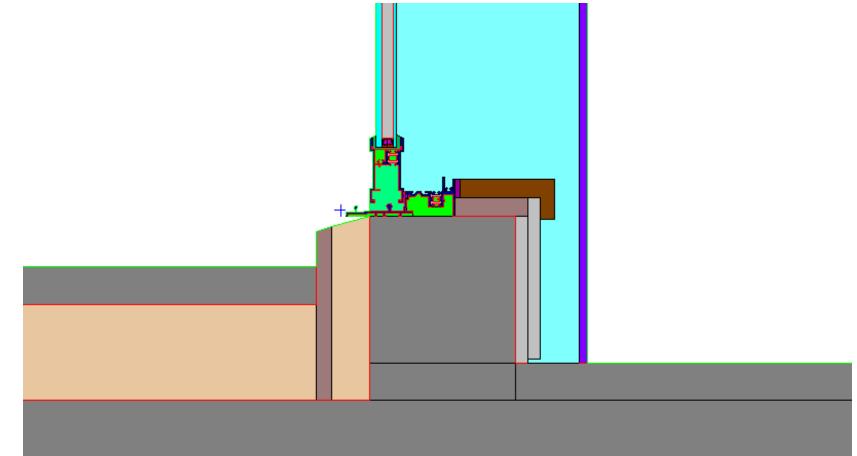






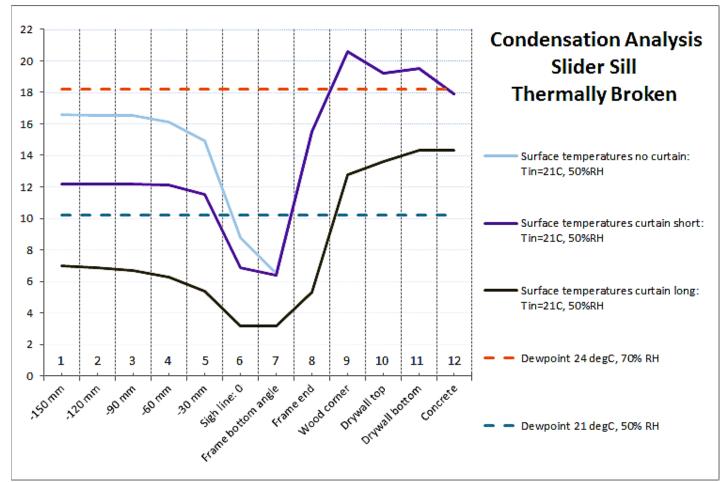








THERM Modeling - Graphical Results





THERM Modeling - Tabulated Results

	Semi-vacant	Moisture loaded	Semi-vacant	Semi-vacant
Outdoor Temperature	-5 degC	-5 degC	-5 degC	
Indoor Temperature	21 degC	24 degC	21 degC	21 degC
Indoor RH	50%	70%	50%	50%
Curtain	open	open	Short closed	Long closed
Indoor dewpoint	10.2 degC	18.2 degC	10.2 degC	10.2 degC
-150 mm	16.6	19.1	12.2	7
-120 mm	16.5	19	12.2	6.9
-90 mm	16.5	19	12.2	6.7
-60 mm	16.1	18.8	12.1	6.3
-30 mm	14.9	17.6	11.5	5.4
Sigh line: 0	8.8	10.4	6.9	3.2
Frame bottom angle	6.5	7.8	6.4	3.2
Frame end	15.5	17.9	15.5	5.3
Wood corner	20.6	23.5	20.6	12.8
Drywall top	19.2	22	19.2	13.6
Drywall bottom	19.5	22.4	19.5	14.3
Concrete	17.9	20.5	17.9	14.3



VENTILATION CONDITIONS OF HOTEL ROOM

ASHRAE 62.1 - 2010

Breathing Zone (Supply) Airflow:

 $V_{bz}=(R_{p}xP_{z}) + (R_{a}xA_{z}) ; R_{p}=5 \text{ cfm/person } R_{a}=0.06 \text{ cfm/ft}^{2}$ $V_{bz}=(5 \text{ cfm/p } x \text{ 2p}) + (0.06 \text{ cfm/ft}^{2} \text{ x } 424 \text{ ft}^{2}) = 35 \text{ cfm}$ $V_{oz}=V_{bz}/E_{z}: E_{z}=0.7 \text{ (Warm floor supply and ceiling return)}$ $V_{oz}=35 \text{ cfm}/0.7 = 50 \text{ cfm}$ Measured Supply Air **36 cfm < 50 cfm**

Exhaust Airflow:

Measured at 27 cfm < 50 cfm requirement

Both outdoor and exhaust airflow **do not** meet ASHRAE 62.1 requirements.



VENTILATION CONDITIONS OF HOTEL ROOM

Fan Coil Unit



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Exterior Wall

Kitchen Fan



Prediction of Thermal Comfort

Hotel Management increased FCU air flow to warm slider; but how is human comfort affected?

Povl Ole Fanger (July 16, 1934 – September 20, 2006): expert in the field of thermal comfort and perception of indoor environments

- Fanger's model relates thermal sensation to physiological variables.
- The model was developed & calibrated with hundreds of individuals that were instrumented & surveyed.

Dr. Rodrigo Mora, P.Eng., BCIT, Building Science Centre of Excellence



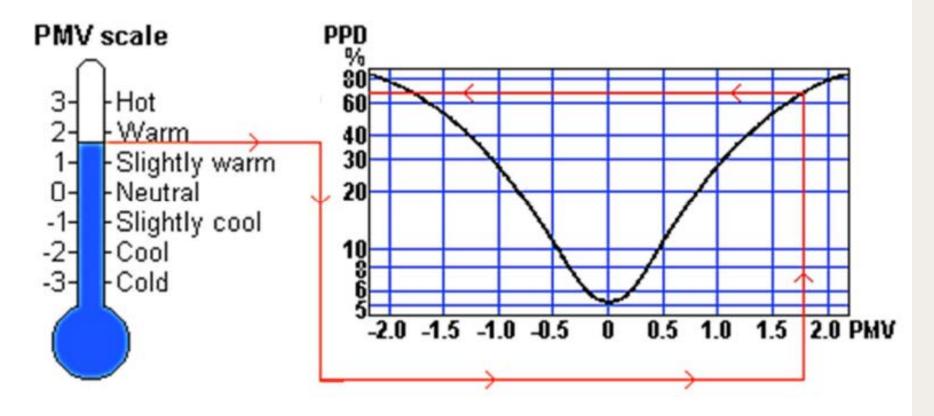
Fanger Model Assumptions

- Uniform airflow; no drafts or spatially localized currents
- Applies to sedentary or moderately elevated activities
- Assumes the whole body is at a uniform temperature (one ball or node)
- Assumes all sweat generated is evaporated
- Applies to indoor spaces that are not naturally conditioned/ventilated)

Does not distinguish between clothed and unclothed portions of the body (clothing asymmetries) - uncovered skin is more sensitive Dr. Rodrigo Mora, P.Eng., BCIT, Building Science Centre of Excellence



Fanger Model – Output



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Fanger Model Inputs

- Relative Humidity: 47%
- Mean Radiant Temperature (MRT): 20°C
- Clothing Insulation (Icl): 0.75 clo (sweatpants and a long sleeve shirt) per ASHRAE 55
- Metabolic Rate: 1.1 met (sitting, reading, typing on a laptop) per ASHRAE 55
- Input parameters: Air temperature and air velocity (however air flow assumes cooling effect)



Fanger Model - Thermal Comfort Results

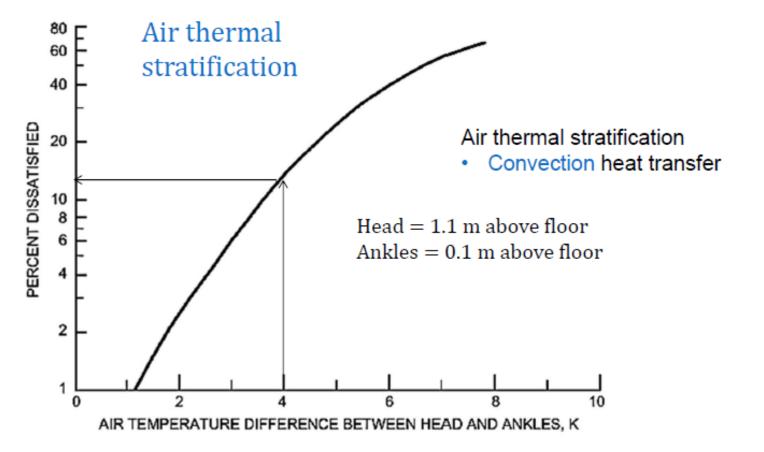
Scenario	Air Temp (°C)	PPD	Commentary	
Semi-vacant	21	24	Usually a little cool	
Fan Coil	25	11	More comfortable but comes with increased air flow	

Fan coil units have three settings, with the highest setting having the most impact on the sliding door

- Unfortunately, local air velocities were > 1 m/s
- Therefore, use of fan coil may assist in warming the sliding door but may create annoyingly drafty conditions



Fanger Model – Limitations (assumes uniform air temperature)



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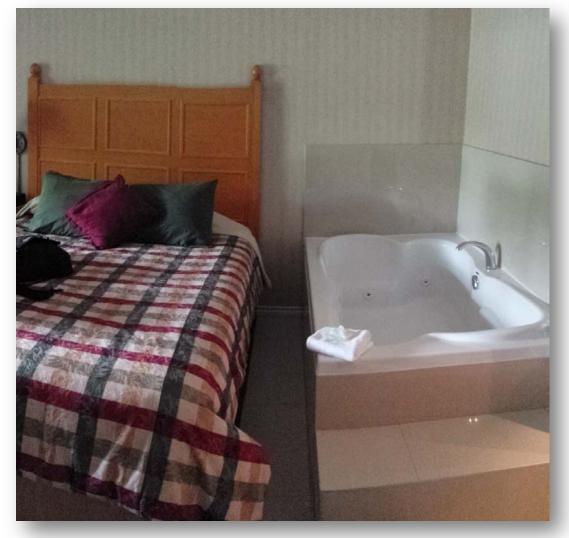
Inherent challenge with hotel units

- 솪 Glazing
- Curtains
- Heating **4b**
- Size 촱
- 4 Layout

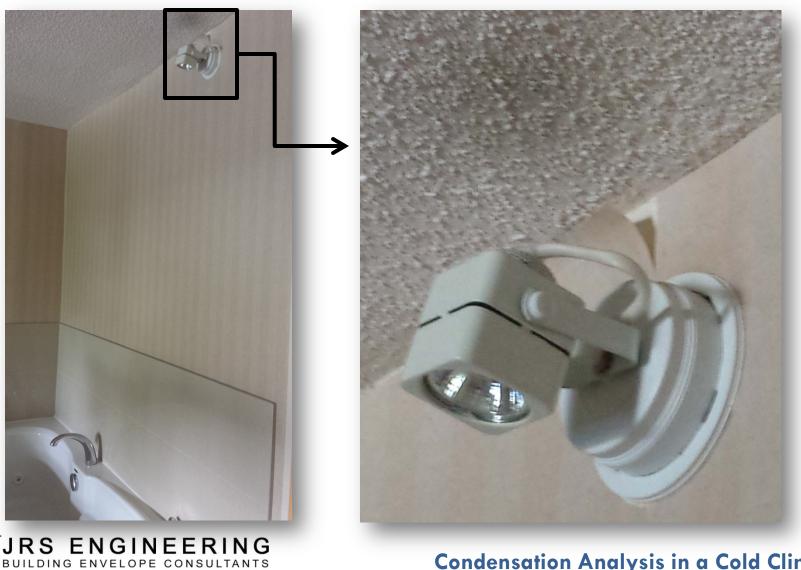




Really?







Multi-tasking





CONTAM is multi-zone airflow and contaminant transport analysis software.

Major Model/Software Assumptions

- Air flow, temperature and pressure is uniform and constant throughout – well mixed with no localized air flow
- Air leakage is uniformly distributed
- Does not consider heat transfer temperature is only considered as it relates to air movement (e.g. pressure differences, stack effect)

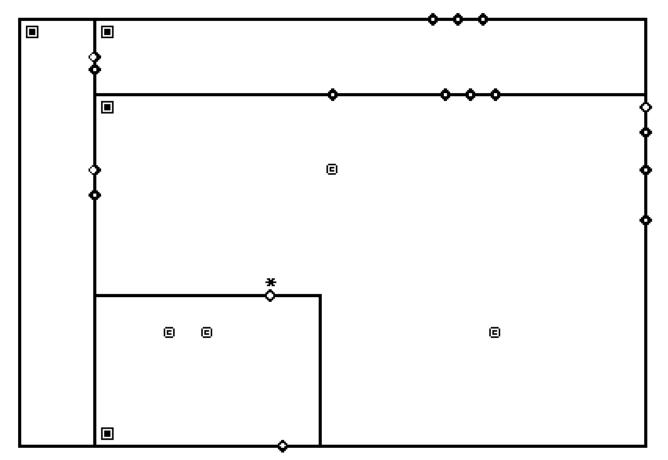


<u>Objective</u>

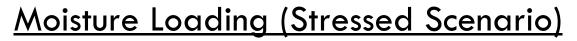
Quantitatively comment on if the humidity problem can be mitigated by increasing the supply air and/or increasing the capacity of the bathroom exhaust fan.

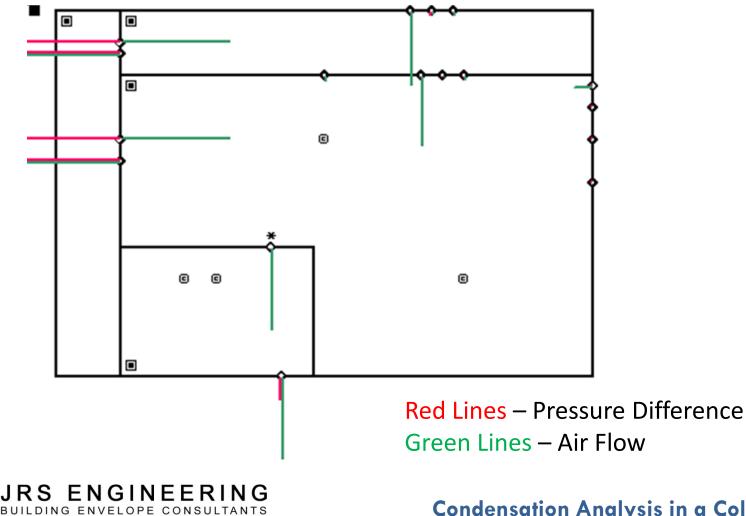




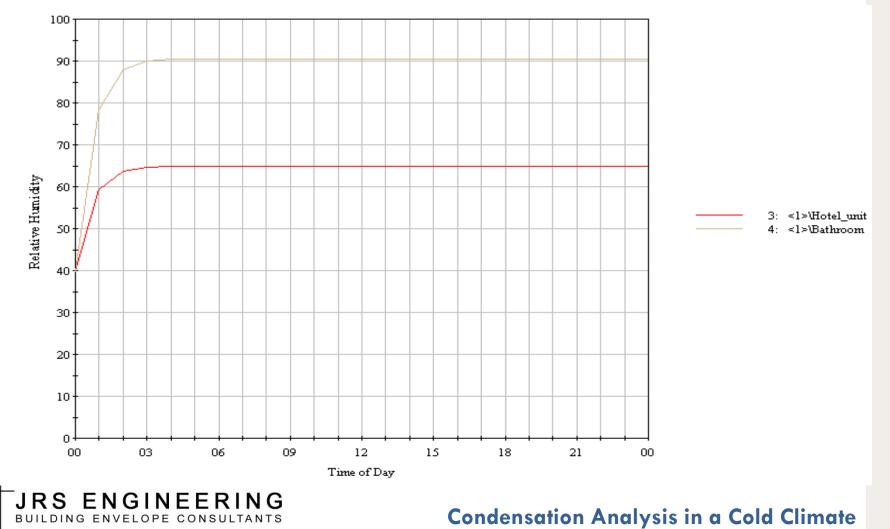




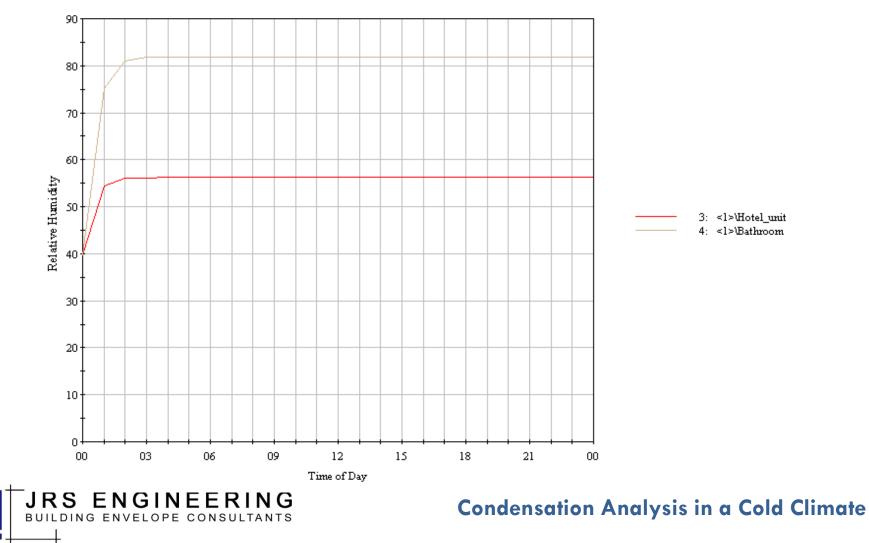




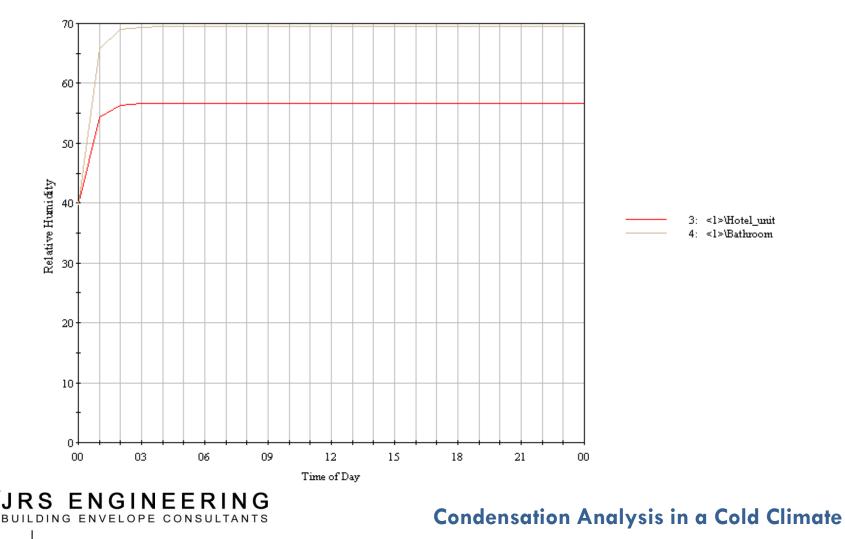
Stressed Condition at Existing Flow Rates



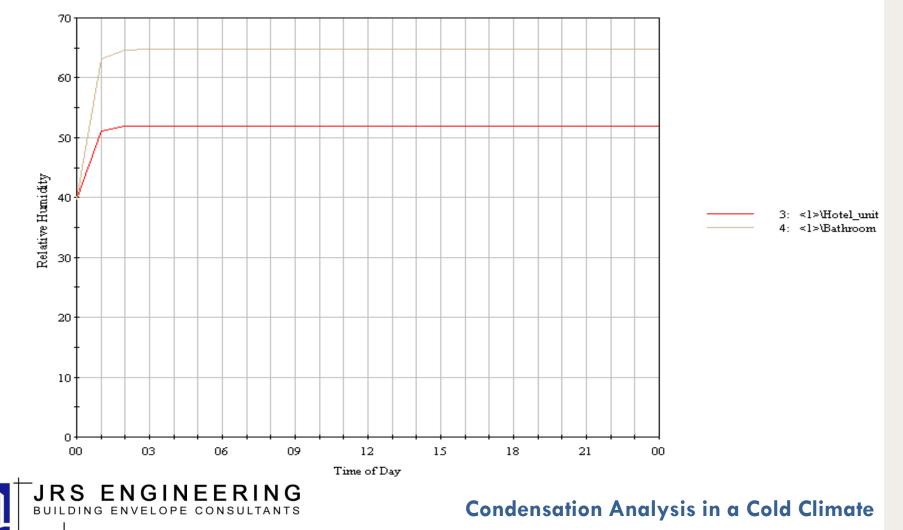
Double Supply Air



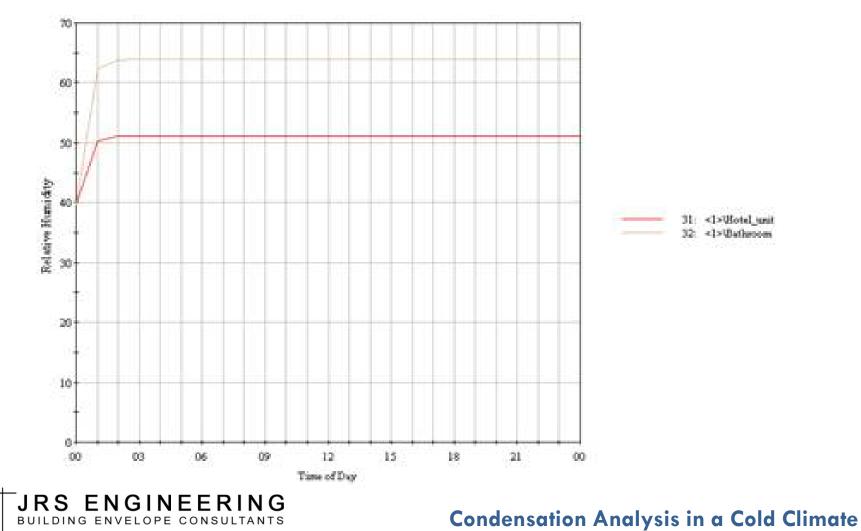
Double Exhaust Flow



Doubled Supply and Exhaust Flow Rates



Stack Effect





Summary Table

Condition	Relative Humidity (%)	
	Hotel Unit	Bathroom
Moisture Loaded	65	91
Supply Air Doubled	57	82
Exhaust Flow Doubled	57	69
Supply and Exhaust Doubled	52	65
With Stack Effect	51	64



The problem has multiple origins, each of which is periodic, seasonal and not independently significant.

<u>Therefore, the solution must also multi-faceted:</u>

- 1) Ventilation Reduce humidity levels in the general vicinity of condensing surfaces.
- 2) Temperature Increase temperature of condensing surfaces.



RECOMMENDATIONS

- 1) Keep heavy drapes open when not in use.
- 2) Trim bottom of curtains.
- 3) Replace weather-stripping gaskets.
- 4) Increase air speed of fan coil unit.
- 5) Balance the HVAC system.
- 6) Install new exhaust fans in bathrooms with an option to increase airflow (e.g. humidistat, movement sensor, on-demand, etc.).
- 7) Install baseboard heaters and with new slider design.



Thanks to the following who helped contribute to this work:

Adam Jarolim, ElT Dr. Rodrigo Mora, P.Eng.

QUESTIONS?



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